

1           Smoothness-Increasing Accuracy-Conserving (SIAC) Filters for  
2         Derivative Approximations of discontinuous Galerkin (DG) Solutions  
3         over Nonuniform Meshes and Near Boundaries

4           X. Li<sup>a,1</sup>, J.K. Ryan<sup>b,1,\*</sup>, R.M. Kirby<sup>c,2</sup>, C. Vuik<sup>a</sup>

5           <sup>a</sup>*Delft Institute of Applied Mathematics, Delft University of Technology, Delft, Netherlands.*

6           <sup>b</sup>*School of Mathematics, University of East Anglia, Norwich, UK.*

7           <sup>c</sup>*School of Computing, University of Utah, Salt Lake City, Utah, USA.*

---

8         **Abstract**

Accurate approximations for the derivatives are usually required in many application areas such as biomechanics, chemistry and visualization applications. With the help of Smoothness-Increasing Accuracy-Conserving (SIAC) filtering, one can enhance the derivatives of a discontinuous Galerkin solution. However, current investigations of derivative filtering are limited to uniform meshes and periodic boundary conditions, which do not meet practical requirements. The purpose of this paper is twofold: to extend derivative filtering to nonuniform meshes and propose position-dependent derivative filters to handle filtering near the boundaries. Through analyzing the error estimates for SIAC filtering, we extend derivative filtering to nonuniform meshes by changing the scaling of the filter. For filtering near boundaries, we discuss the advantages and disadvantages of two existing position-dependent filters and then extend them to position-dependent derivative filters, respectively. Further, we prove that with the position-dependent derivative filters, the filtered solutions can obtain a better accuracy rate compared to the original discontinuous Galerkin approximation with arbitrary derivative orders over nonuniform meshes. One- and two-dimensional numerical results are provided to support the theoretical results and demonstrate that the position-dependent derivative filters, in general, enhance the accuracy of the solution for both uniform and nonuniform meshes.

9         **Keywords:** Discontinuous Galerkin method, Post-processing, SIAC filtering, Superconvergence,  
10       Nonuniform meshes, Boundaries

---

11       **1. Introduction**

12       In many cases, one can argue persuasively that the changes in values of a function are often more  
13       import than the values themselves, such as exhibited by streamline integration of fields. Therefore, an  
14       accurate derivative approximation is often required in many areas such as biomechanics, optimization,  
15       chemistry and visualization applications. However, computing derivatives of discontinuous Galerkin  
16       approximations is challenging because the DG solution only has weak continuity at element boundaries.  
17       This means that the strong form of derivatives for a DG solution technically do not hold at element  
18       boundaries, and computing the derivative directly does not always produce accurate results. For exam-  
19       ple, naive and careless use of the derivatives of the discontinuous Galerkin solution directly to streamline

---

\*Corresponding author

Email addresses: X.Li-2@tudelft.nl (X. Li), Jennifer.Ryan@uea.ac.uk (J.K. Ryan), kirby@cs.utah.edu  
(R.M. Kirby), C.Vuik@tudelft.nl (C. Vuik)

<sup>1</sup>Supported by the Air Force Office of Scientific Research (AFOSR), Air Force Material Command, USAF, under grant numbers FA8655-13-1-3017.

<sup>2</sup>Supported by the Air Force Office of Scientific Research (AFOSR), Computational Mathematics Program (Program Manager: Dr. Fariba Fahroo), under grant number FA9550-12-1-0428.

20 integration can produce inconsistent results with the exact solution [1]. Once derivatives are needed  
21 near the boundaries, the difficulty increases since the solution often has less regularity in those regions.

22 In order to obtain accurate approximations for the derivatives of discontinuous Galerkin (DG) so-  
23 lutions, this paper focuses on using the so-called Smoothness-Increasing Accuracy-Conserving class of  
24 filters. As the name implies, SIAC filtering can increase the smoothness of DG solutions, and this  
25 smoothness-increasing property helps to enhance the accuracy of derivatives of DG solutions. Before  
26 giving context to what we will propose, we first review the currently existing SIAC and derivative SIAC  
27 filters. The source of SIAC filtering is considered to be the superconvergence extraction technique in-  
28 troduced by [2] for finite element solutions of elliptic problems. The extension for DG methods of linear  
29 hyperbolic equations given in [3]. In an ideal situation, by applying SIAC filtering, the accuracy order  
30 of the filtered DG approximation can improve from  $k + 1$  to  $2k + 1$ . The concept of the derivative filter  
31 was introduced in [4] for finite element methods and [5] for DG methods. With the derivative filter, the  
32 filtered solution maintains an accuracy order of  $2k + 1$  regardless of the derivative order. However, the  
33 previous investigations of derivative filtering have two major limitations: the requirement of a uniform  
34 meshes and periodic boundary conditions.

35 The purpose of this paper is to overcome these two limitations. We propose position-dependent  
36 derivative filters to approximate the derivatives of the discontinuous Galerkin solution over nonuniform  
37 meshes and near boundaries. Our main contributions are:

38 **Nonuniform Meshes.** Filtering over nonuniform meshes has always been a significant challenge  
39 for SIAC filtering since the  $2k + 1$  accuracy order is no longer guaranteed in general. Most of previous  
40 work for nonuniform meshes (such as [6, 7, 8]) only considered a particular family of nonuniform meshes,  
41 smoothly-varying meshes. Among these works, only [7] mentioned derivatives over nonuniform meshes.  
42 It discussed the challenges of derivative filtering over nonuniform meshes and presented preliminary  
43 results concerning smooth-varying meshes. In this paper, we propose a method for arbitrary nonuniform  
44 meshes: using the scaling  $H = h^\mu$  for filtering over nonuniform meshes. We can not guarantee that  
45 the derivative filtering can improve the derivatives of DG solutions to accuracy order of  $2k + 1$ , but we  
46 prove that a higher convergence rate (compared to DG solution) is still obtained. Further, the numerical  
47 examples suggest that the accuracy is improved once the mesh is sufficiently refined.

48 **Boundaries.** First, we point out that previously there was no derivative filter that could be used  
49 near boundaries except for periodic meshes. Without considering derivatives, there are three existing  
50 position-dependent filters that can be used to handle boundary regions, see [8, 9, 10]. Two of them,  
51 [9, 10], are constructed by only using central B-splines. They showed good performance over uniform  
52 meshes. The position-dependent filter recently introduced in [8] was aimed at nonuniform meshes. It  
53 uses  $2k + 1$  central B-splines and an extra general B-spline. The results in [8] suggested that adding  
54 the extra general B-spline improves the performance of the position-dependent filter over nonuniform  
55 meshes compared to using only central B-splines. In this paper, we extend the position-dependent filter  
56 [10] (referred to as SRV filter) and the new position-dependent filter [8] (referred to as RLKV filter)  
57 to position-dependent derivative filters. Then, we discuss the advantages and disadvantages of these  
58 position-dependent derivative filters over uniform and nonuniform meshes. For nonuniform meshes, we  
59 prove that by using the position-dependent derivative filtering, the convergence rate of the derivatives  
60 of the DG solution can be improved. Numerical comparisons over uniform and nonuniform meshes  
61 also demonstrate that the derivative filtered solutions are more accurate than the derivatives of DG  
62 approximations.

63 Our new contributions are:

- 64 • Testing the position-dependent derivative filters for uniform meshes, which has never been done  
65 before;
- 66 • Applying the symmetric and position-dependent derivative filters over different nonuniform meshes.

67 This paper is organized as follows. In Section 2, we first review properties of the discontinuous  
68 Galerkin solution and its derivatives. Then, we introduce the symmetric and position-dependent filters.

69 Lastly, we show the symmetric derivative filter over uniform meshes. The symmetric and position-  
 70 dependent derivative filters over nonuniform meshes are presented in Section 3 with theoretical error  
 71 estimations. Numerical results over uniform and nonuniform one-dimensional meshes are given in Section  
 72 4. Nonuniform two-dimensional quadrilateral meshes are considered in Section 5. We present conclusions  
 73 in Section 6.

## 74 2. Background

75 In this section, we first briefly review the basic features of discontinuous Galerkin methods and the  
 76 properties related to derivatives. Then, we present the relevant background of Smoothness-Increasing  
 77 Accuracy-Conserving filters.

### 78 2.1. DG Approximation and Its Derivatives

79 Consider a multi-dimensional linear hyperbolic equation

$$80 u_t + \sum_{i=1}^d A_i u_{x_i} + A_0 u = 0, \quad u(\mathbf{x}, 0) = u_0(\mathbf{x}), \quad (\mathbf{x}, t) \in \Omega \times (0, T], \quad \Omega \subset \mathbb{R}^d, \quad (2.1)$$

80 where the initial condition  $u_0(\mathbf{x})$  is a sufficiently smooth function and the coefficients  $A_i$  are constants.  
 81 The details of discontinuous Galerkin methods for hyperbolic equations can be found in [11, 12]. Here,  
 82 we skip the details and write the DG approximation directly as

$$83 u_h(\mathbf{x}, t) = \sum_{|\ell|=0}^k u_K^\ell(t) \varphi_K^\ell(\mathbf{x}), \quad \text{for } \mathbf{x} \in K,$$

83 where  $k$  is the highest degree of approximation polynomial, and  $\varphi_K^\ell$  is the multi-dimensional piecewise  
 84 polynomial basis function of degree  $\ell$ ,  $\ell = (\ell_1, \dots, \ell_d)$  is a multi-index, polynomial inside element  $K$   
 85 and zero outside  $K$ . Here we choose scaled Legendre polynomials for simplicity. The mesh elements  $K$   
 86 can be either uniform or nonuniform, and the mesh size is represented as  $h_K$  ( $h$  for uniform meshes).

87 A well-known feature of the DG approximation is that the use of a piecewise polynomial basis leads  
 88 to superconvergence. However, by using a piecewise polynomial basis, the solution  $u_h$  is discontinuous  
 89 at the interface of the elements, which is the main challenge to defining the global derivatives of the DG  
 90 approximation. Alternatively, we can define the local derivatives of  $u_h$  in the interior of each element  
 91 by

$$92 \partial_x^\alpha u_h(\mathbf{x}, t) = \sum_{|\ell|=0}^k u_K^\ell(t) \partial_x^\alpha \varphi_K^\ell(\mathbf{x}), \quad \text{for } \mathbf{x} \in K, \quad (2.2)$$

92 where  $\alpha = (\alpha_1, \dots, \alpha_d)$  is an arbitrary multi-index. Equation (2.2) is an approximation of  $\partial_x^\alpha u$ , but it  
 93 is only a local derivative, and the convergence rate in Equation (2.3) is not satisfied. Unlike the general  
 94 DG approximation, which has the convergence rate of  $k+1$ , with each successive derivative, one order  
 95 of accuracy is lost,

$$96 \|\partial_x^\alpha u - \partial_x^\alpha u_h\|_0 \sim \mathcal{O}(h^{k+1-|\alpha|}). \quad (2.3)$$

96 This means  $|\alpha| \leq k$ , since the  $(k+1)$ th derivative is just zero. In order to obtain a global and accurate  
 97 derivative of the DG approximation, we can increase its smoothness by using SIAC filtering. Since the  
 98 filtered solutions are more smooth and have higher accuracy order, this filtering technique allows us to  
 99 obtain derivatives for  $|\alpha| > k$ . We emphasize that the ability of calculating derivatives for  $|\alpha| > k$  is a  
 100 unique benefit of using SIAC filtering.

101    2.2. *SIA C Filter*

102    Smoothness-Increasing Accuracy-Conserving filtering is based on a postprocessing technique first  
 103    demonstrated by Bramble and Schatz [2] for finite element methods to obtain a better approximation.  
 104    Later, in [3], this technique was extended to DG methods. In the one-dimensional case, the filtered  
 105    approximation  $u_h^*$  is given by

$$u_h^*(x) = K_h^{(r+1,k+1)} \star u_h(x), \quad (2.4)$$

106    and

$$\|u - u_h^*\|_0 \leq Ch^{2k+1},$$

107    where the symmetric filter  $K^{(r+1,k+1)}$  is a linear combination of the central B-splines,

$$K^{(r+1,k+1)}(x) = \sum_{\gamma=0}^r c_\gamma^{(r+1,k+1)} \psi^{(k+1)} \left( x + \frac{r}{2} - \gamma \right). \quad (2.5)$$

108    and the scaled filter  $K_h$  is given by formula  $K_h(x) = \frac{1}{h} K(\frac{x}{h})$ . In [2, 3], the number of B-splines is  
 109     $r + 1 = 2k + 1$ . The coefficients  $c_\gamma^{(r+1,k+1)}$  are calculated by requiring the filter to reproduce the  
 110    polynomials by convolution

$$K^{(r+1,k+1)} \star p = p, \quad p = 1, x, \dots, x^r.$$

Here, the central B-splines are constructed recursively by

$$\begin{aligned} \psi^{(1)}(x) &= \chi_{[-1/2, 1/2]}(x), \\ \psi^{(\ell+1)}(x) &= \psi^{(1)} \star \psi^{(\ell)}, \quad \ell \geq 1. \end{aligned}$$

111    We note that this symmetric filter is suitable only for the interior region,  $(r + k + 1)/2$  elements away  
 112    from the boundaries of the entire domain since it uses symmetric information around the evaluated  
 113    point. When filtering near the domain boundaries, we need to use position-dependent filters.

114    In the multi-dimensional case, the filter is a tensor product of the one-dimensional filters (2.5) and  
 115    can be written as

$$K_h^{(r+1,k+1)}(\mathbf{x}) = \prod_{i=1}^d K_h^{(r+1,k+1)}(x_i), \quad \mathbf{x} = (x_1, \dots, x_d) \in \mathbb{R}^d,$$

116    with the scaled filter  $K_h^{(r+1,k+1)}(\mathbf{x}) = \frac{1}{h^d} K^{(r+1,k+1)} \left( \frac{\mathbf{x}}{h} \right)$ .

117    2.3. *Position-Dependent Filter*

118    There are three position-dependent filters that have been introduced in previous work. Two of the  
 119    three, [9, 10], use only central B-splines. These central B-spline filters have similar structures. Here we  
 120    only discuss the one with better performance, [10], referred to as the SRV filter, in this section. The  
 121    last position-dependent filter use central B-splines, and an extra noncentral B-spline. It was recently  
 122    introduced in [8], and the error of the filtered solution near the boundary is reduced over nonuniform  
 123    meshes compared to the SRV filter. In the following context, we refer to position-dependent filter [8] as  
 124    the RLKV filter.

125    2.3.1. *SRV Filter*

126    The SRV filter using  $4k + 1$  central B-splines was introduced in [10] for uniform meshes. This  
 127    boundary filter demonstrated better behavior in terms of error than the original position-dependent  
 128    filter which uses  $2k + 1$  given by Ryan and Shu in [9]. It changes its support according to the location  
 129    of the point being filtered. For example, at the left boundary, a translation of the filter should be done

so that the support of the filter remains inside the domain (up to the left boundary). The SRV filter for filtering near the boundaries can then be written as

$$K^{(4k+1,k+1)}(x) = \sum_{\gamma=0}^{4k} c_{\gamma}^{(4k+1,k+1)} \psi^{(k+1)}(x - x_{\gamma}(\bar{x})), \quad (2.6)$$

where  $x_{\gamma}$  depends on the location of the evaluation point  $\bar{x}$  and is given by

$$x_{\gamma}(\bar{x}) = -2k + \gamma + \lambda(\bar{x}),$$

with

$$\lambda(\bar{x}) = \begin{cases} \min\{0, -\frac{5k+1}{2} + \frac{\bar{x}-x_{left}}{h}\}, & \bar{x} \in [x_{left}, \frac{x_{left}+x_{right}}{2}), \\ \max\{0, \frac{5k+1}{2} + \frac{\bar{x}-x_{right}}{h}\}, & \bar{x} \in [\frac{x_{left}+x_{right}}{2}, x_{right}]. \end{cases} \quad (2.7)$$

Here  $x_{left}$  and  $x_{right}$  are the left and right boundaries, respectively. In the interior, the symmetric filter uses  $2k+1$  central B-splines. In order to provide a smooth transition between the SRV filter and the symmetric filter, a convex combination was used:

$$u_h^*(x) = \theta(x) \left( K_h^{(2k+1,k+1)} \star u_h \right)(x) + (1 - \theta(x)) \left( K_h^{(4k+1,k+1)} \star u_h \right)(x), \quad (2.8)$$

where  $\theta(x) \in \mathcal{C}^{k-1}$  such that  $\theta = 1$  in the interior and  $\theta = 0$  in the boundary regions. The SRV filter showed good performance over uniform meshes in [10] when a multi-precision package was used. However, recent work [8] showed that the SRV filter was not suitable for nonuniform meshes.

### 2.3.2. RLKV Filter

The performance of the SRV filter strongly depends on three conditions: the problem is linear, the mesh is uniform and the computations are carried out with a multi-precision package (at least quadruple precision). When one of these conditions is not satisfied, the good performance of the SRV filter can no longer be guaranteed. In order to overcome the aforementioned limitations, the RLKV filter was proposed in [8]. This RLKV filter uses  $2k+1$  central B-splines and an extra general B-spline. Near the left boundary, the RLKV filter has the formula

$$K_{\mathbf{T}}^{(2k+2,k+1)}(x) = \underbrace{\sum_{\gamma=0}^{2k} c_{\gamma}^{(2k+2,k+1)} \psi_{\mathbf{T}(\gamma)}^{(k+1)}(x)}_{\text{Position-dependent filter with } 2k+1 \text{ central B-splines}} + \underbrace{c_{2k+1}^{(2k+2,k+1)} \psi_{\mathbf{T}(2k+1)}^{(k+1)}(x)}_{\text{General B-spline}}, \quad (2.9)$$

where  $\mathbf{T}$  is the knot matrix defined in [8]. This knot matrix is a  $(2k+2) \times (k+2)$  matrix such that each row,  $\mathbf{T}(i) = [T(i,0), \dots, T(i,k+1)]$  ( $i = 0, \dots, 2k+1$ ), of the matrix is a knot sequence with  $k+2$  elements that are used to create the B-spline  $\psi_{\mathbf{T}(\gamma)}^{(k+1)}(x)$ . Let  $\mathbf{T}(i, j_0 : j_1)$  represents the knot sequence  $[T(i, j_0), T(i, j_0+1), \dots, T(i, j_1)]$ , then the B-spline can be constructed by the following recurrence relation [13]:

$$\psi_{\mathbf{T}(i,0:\ell)}^{(\ell)}(x) = \begin{cases} \chi_{[T(i,0), T(i,1))} & \text{for } \ell = 1; \\ \frac{x-T(i,0)}{T(i,\ell-1)-T(i,0)} \psi_{\mathbf{T}(i,0:\ell-1)}^{(\ell-1)}(x) + \left(1 - \frac{x-T(i,1)}{T(i,\ell)-T(i,1)}\right) \psi_{\mathbf{T}(i,1:\ell)}^{(\ell-1)}(x) & \text{for } \ell > 1. \end{cases}$$

We note that the definition above provides more flexibility than the previous central B-spline notation, where  $\mathbf{T}(i)$  are sequences of equidistant knots. Assume that we want to filter the point  $\bar{x}$  which is located near the left boundary, then  $\mathbf{T}$  is given by,

$$T(i,j) = \begin{cases} -3k-1+j+i+\frac{\bar{x}-x_{left}}{h}, & 0 \leq i \leq 2k, 0 \leq j \leq k+1; \\ \frac{\bar{x}-x_{left}}{h} + \min\{j-1, 0\}, & i = 2k+1, 0 \leq j \leq k+1; \end{cases} \quad (2.10)$$

155 similarly near the right boundary the knot sequence is given by

$$T(i, j) = \begin{cases} \frac{\bar{x} - x_{right}}{h} + \max\{j - k, 0\}, & i = 0, 0 \leq j \leq k + 1; \\ i + j - 1 + \frac{\bar{x} - x_{right}}{h}, & 1 \leq i \leq 2k + 1, 0 \leq j \leq k + 1. \end{cases} \quad (2.11)$$

156 More details of this position-dependent filter can be found in [8].

#### 157 2.4. Symmetric Derivative Filter: Uniform Meshes

158 Smoothness-Increasing Accuracy-Conserving filtering is named after its improvement of the smooth-  
159 ness of the filtered approximation. Using the filter in equation (2.5), the filtered solution is a  $\mathcal{C}^{k-1}$   
160 function. One can see that the smoothness is significantly improved from the original weakly con-  
161 tinuous solution. By taking advantage of the improved smoothness, we can obtain better derivative  
162 approximations.

163 Derivative filtering over uniform meshes was introduced in [5, 4]. In these papers, the authors  
164 identified two ways to calculate the derivatives. The first method is a direct calculation of the derivatives  
165 of the filtered solution (2.4). The convergence rate of the filtered solution is higher than the derivatives  
166 of the DG approximation itself, but the accuracy order decreases and oscillations in the error increase  
167 with each successive derivative. The second method is employed to maintain a fixed accuracy order  
168 regardless of the derivative order. In order to calculate the  $\alpha$ th derivative of the DG approximation  
169 without losing any accuracy order, we have to use higher-order central B-splines to construct the filter,

$$K^{(r+1,k+1+\alpha)}(x) = \sum_{\gamma=0}^r c_{\gamma}^{(r+1,k+1+\alpha)} \psi^{(k+1+\alpha)}(x + \frac{r}{2} - \gamma). \quad (2.12)$$

170 Notice that the order of the B-splines is now  $k + 1 + \alpha$  instead of  $k + 1$  in (2.5), and the filtered  
171 solution becomes a  $\mathcal{C}^{k-1+\alpha}$  function. Then we can write the  $\alpha$ th derivative of the symmetric kernel as  
172  $\frac{d^\alpha}{dx^\alpha} K_h^{(r+1,k+1+\alpha)}(x) = \partial_h^\alpha \tilde{K}_h^{(r+1,k+1,\alpha)}$ , where

$$\tilde{K}_h^{(r+1,k+1,\alpha)} = \sum_{\gamma=0}^r c_{\gamma}^{(r+1,k+1+\alpha)} \psi_h^{(k+1)}(x + \frac{r}{2} - \gamma).$$

173 By the property of convolution,

$$\partial_x^\alpha u_h^* = \partial_x^\alpha \left( K_h^{(r+1,k+1+\alpha)} * u_h \right) = \left( \frac{d^\alpha}{dx^\alpha} K_h^{(r+1,k+1+\alpha)} \right) * u_h = \left( \partial_h^\alpha \tilde{K}_h^{(r+1,k+1,\alpha)} \right) * u_h. \quad (2.13)$$

174 For uniform meshes, [5] showed the filtered solution (2.13) has  $2k + 1$  superconvergence rate regardless  
175 of the derivative order  $\alpha$

$$\| \partial_x^\alpha u - \partial_x^\alpha u_h^* \|_0 \sim \mathcal{O}(h^{2k+1}).$$

176 Unfortunately, these methods are limited to uniform meshes. For nonuniform meshes, SIAC filtering  
177 becomes complicated, and derivative SIAC filtering is more difficult. If we naively apply the same deriva-  
178 tive filtering technique over nonuniform meshes, we will lose accuracy from  $\mathcal{O}(h^{2k+1})$  to  $\mathcal{O}(h^{k+1-\alpha})$  since  
179 over nonuniform meshes the divided differences of the DG solution no longer have the superconverge-  
180 nce property. In the following section, we will address nonuniform meshes by adjusting the scaling of the  
181 SIAC filter.

### 182 3. Derivative Filter: Nonuniform Meshes and Near Boundaries

#### 183 3.1. Symmetric Derivative Filter: Nonuniform Meshes

184 A brief introductory description of symmetric derivative filtering over nonuniform meshes can be  
185 found in [7]. It discusses the challenges of symmetric derivative filtering over nonuniform meshes and  
186 gives preliminary results for smoothly-varying meshes (an affine mapping of a uniform mesh [6]). In  
187 order to develop derivative filtering for arbitrary nonuniform meshes, we first present some useful  
188 lemmas.

189 **Lemma 3.1** (Bramble and Schatz [2]). *Let  $\Omega_0 \subset\subset \Omega_1$  and  $s$  be an arbitrary but fixed nonnegative  
190 integer. Then for  $u \in H^s(\Omega_1)$ , there exists a constant  $C$  such that*

$$\|u\|_{0,\Omega_0} \leq C \sum_{|\alpha| \leq s} \|D^\alpha u\|_{-s,\Omega_1}.$$

**Lemma 3.2.** *Let  $u$  be the exact solution to the linear hyperbolic equation*

$$\begin{aligned} u_t + \sum_{i=1}^d A_i u_{x_i} + A_0 u &= 0, \quad \mathbf{x} \in \Omega \times (0, T], \\ u(\mathbf{x}, 0) &= u_0(\mathbf{x}), \quad \mathbf{x} \in \Omega, \end{aligned} \tag{3.1}$$

191 where the initial condition  $u_0(\mathbf{x})$  is a sufficiently smooth function and the coefficients  $A_i$  are constants.  
192 Here,  $\Omega \subset \mathbb{R}^d$ . Let  $u_h$  be the DG approximation over a nonuniform mesh with periodic boundary  
193 condition. Denote  $\Omega_0 \subset\subset \Omega_1 \subset\subset \Omega$ ,  $\ell \geq k+1$ . The negative order norm estimation of  $u - u_h$  satisfies,

$$\|(u - u_h)(T)\|_{-\ell,\Omega_1} \leq Ch^{2k+1},$$

194 and

$$\|\partial_H^\alpha(u - u_h)(T)\|_{-\ell,\Omega_0} \leq C_\alpha h^{2k+1} H^{-|\alpha|},$$

195 where  $\alpha = (\alpha_1, \dots, \alpha_d)$  is an arbitrary multi-index and  $H$  is the scaling of the divided difference operator  
196  $\partial_H^\alpha$ .

197 *Proof.* The proof of the negative order norm estimation was given in [3] and the divided difference estimation was presented as a hypotheses. The proof is trivial and therefore we only give a proof for  $d = 1$  case.

200 Set  $\Omega_0$  such that  $\Omega_0 + \left[-\frac{|\alpha|H}{2}, \frac{|\alpha|H}{2}\right] \subset \Omega_1$ . Consider the first divided difference, by the definition  
201 of the negative order norm, we have

$$\begin{aligned} \|\partial_H(u - u_h)\|_{-\ell,\Omega_0} &= \sup_{\Phi \in \mathcal{C}_0^\infty(\Omega_0)} \left( \frac{\left( (u - u_h)(x + \frac{H}{2}), \Phi \right) - \left( (u - u_h)(x - \frac{H}{2}), \Phi \right)}{H \|\Phi\|_{\ell,\Omega_0}} \right), \\ &\leq \sup_{\Phi \in \mathcal{C}_0^\infty(\Omega_0)} \frac{\left( (u - u_h)(x + \frac{H}{2}), \Phi \right)}{H \|\Phi\|_{\ell,\Omega_0}} + \sup_{\Phi \in \mathcal{C}_0^\infty(\Omega_0)} \frac{\left( (u - u_h)(x - \frac{H}{2}), \Phi \right)}{H \|\Phi\|_{\ell,\Omega_0}}, \\ &\leq \frac{2}{H} \|u - u_h\|_{-\ell,\Omega_1}. \end{aligned}$$

202 By induction, we have

$$\|\partial_H^\alpha(u - u_h)(T)\|_{-\ell,\Omega_0} \leq C_\alpha h^{2k+1} H^{-|\alpha|},$$

203 where  $C_\alpha = 2^{|\alpha|} C$ . The proof is similar for  $d > 1$  case.  $\square$

204 Lemma 3.2 demonstrates the optimal accuracy order estimation of the divided differences of the DG  
205 approximation in the sense that the nonuniform mesh is arbitrary [3, 14].

206 **Theorem 3.3.** *Under the same conditions as in Lemma 3.2, let  $K^{(r+1,k+1+\alpha)}$  be the symmetric derivative filter given in (2.12). Denote  $\Omega_0 + 2\text{supp}(K_H^{(r+1,k+1+\alpha)}) \subset\subset \Omega_1 \subset\subset \Omega$ . Then, for general nonuniform meshes, we have*

$$\|\partial_x^\alpha u - \partial_x^\alpha \left( K_H^{(r+1,k+1+\alpha)} \star u_h \right)\|_{0,\Omega_0} \leq Ch^{\frac{r+1}{r+k+2+\alpha}(2k+1)},$$

209 where  $H = h^\mu$  and  $\mu = \frac{2k+1}{r+k+2+\alpha}$ .

210 *Proof.* Set  $\Omega_{1/2}$  such that

$$\Omega_0 + \text{supp}(K_H^{(r+1,k+1+\alpha)}) \subset \Omega_{1/2}, \quad \text{and} \quad \Omega_{1/2} + \text{supp}(K_H^{(r+1,k+1+\alpha)}) \subset \Omega_1.$$

211 By applying Lemma 3.1 and Lemma 3.2, we have

$$\begin{aligned} & \left\| \partial_x^\alpha u - \partial_x^\alpha \left( K_H^{(r+1,k+1+\alpha)} \star u_h \right) \right\|_{0,\Omega_0} \\ & \leq \left\| \partial_x^\alpha u - K_H^{(r+1,k+1+\alpha)} \star \partial_x^\alpha u \right\|_{0,\Omega_0} + \left\| \partial_x^\alpha \left( K_H^{(r+1,k+1+\alpha)} \star (u - u_h) \right) \right\|_{0,\Omega_0} \\ & \leq C_0 H^{r+1} + C_1 \sum_{|\beta| \leq k+1} \left\| \partial_x^{\alpha+\beta} \left( K_H^{(r+1,k+1+\alpha)} \star (u - u_h) \right) \right\|_{-(k+1),\Omega_{1/2}} \\ & = C_0 H^{r+1} + C_1 \sum_{|\beta| \leq k+1} \left\| \left( \tilde{K}_H^{(r+1,k+1-\beta,\alpha+\beta)} \star \partial_H^{\alpha+\beta} (u - u_h) \right) \right\|_{-(k+1),\Omega_{1/2}} \\ & = C_0 H^{r+1} + C_1 \sum_{|\beta| \leq k+1} \left\| \tilde{K}_H^{(r+1,k+1-\beta,\alpha+\beta)} \right\|_{L^1} \left\| \partial_H^{\alpha+\beta} (u - u_h) \right\|_{-(k+1),\Omega_1} \\ & \leq C_0 H^{r+1} + C_2 h^{2k+1} H^{-(k+1+\alpha)}, \end{aligned}$$

212 Let the scaling  $H = h^\mu$  such that

$$H^{r+1} = h^{2k+1} H^{-(k+1+\alpha)}.$$

213 We then have that  $\mu = \frac{2k+1}{r+k+2+\alpha}$  and

$$\left\| \partial_x^\alpha u - \partial_x^\alpha \left( K_H^{(r+1,k+1+\alpha)} \star u_h \right) \right\|_{0,\Omega_0} \leq C h^{\frac{r+1}{r+k+2+\alpha}(2k+1)}.$$

214

□

215 **Remark 3.1** (Discussion of the Number of B-splines). The filter given in (2.12) uses  $(r+1)$  B-splines.  
216 Theorem 3.3 implies that by increasing the value of  $r$ , one can increase the value of  $\frac{r+1}{r+k+2+\alpha}$ , and then  
217 approximate the superconvergence rate  $2k+1$  as close as we want and regardless of the derivative order  $\alpha$ .  
218 However, increasing the value of  $r$  presents a serious inconvenience for computational implementation.  
219 For example, while  $r \gg 2k$ , a multi-precision package is required during the computation process, [8].  
220 Another disadvantage is that the support size of the filter,  $(r+k+1+\alpha)h^\mu$ , increases with  $r$  [3]. The  
221 increased support size means the convolution involves more DG elements and that the computational  
222 cost is increases as well. For nonderivative filtering, we usually keep  $r = 2k$ , but there is another  
223 consideration for derivative filtering. We notice that the accuracy order decreases with the derivative  
224 order  $\alpha$  if we keep  $r = 2k$ . One solution is to eliminate the negative effect of the derivative order  $\alpha$  is to  
225 use  $r = 2(k+\alpha)$  instead of  $r = 2k$ . However, our experience shows that the benefit of using  $r = 2(k+\alpha)$   
226 is limited. It slightly improves the accuracy and smoothness, but increases the computational cost. In  
227 this paper, we will focus on using  $r = 2k$  for nonuniform meshes.

### 228 3.2. Position-Dependent Derivative Filter

229 In the previous section, we discussed the symmetric derivative filtering over nonuniform meshes. As  
230 we mentioned before, in order to handle boundary regions, we need to use position-dependent filters.  
231 In this section, we extend two position-dependent filters to position-dependent derivative filters.

#### 232 3.2.1. Derivative SRV Filter

233 Since the SRV filter uses only central B-splines, we can easily extend it to the derivative SRV filter  
234 by increasing the order of B-splines from  $k+1$  in (2.6) to  $k+1+\alpha$

$$K^{(4k+1,k+1+\alpha)}(x) = \sum_{\gamma=0}^{4k} c_\gamma^{(4k+1,k+1+\alpha)} \psi^{(k+1+\alpha)}(x - x_\gamma), \quad (3.2)$$

<sup>235</sup> and adjust the shift function  $\lambda(\bar{x})$  (2.7) to

$$\lambda(\bar{x}) = \begin{cases} \min\{0, -\frac{5k+1+\alpha}{2} + \frac{\bar{x}-x_{left}}{h}\}, & \bar{x} \in [x_{left}, \frac{x_{left}+x_{right}}{2}), \\ \max\{0, \frac{5k+1+\alpha}{2} + \frac{\bar{x}-x_{right}}{h}\}, & \bar{x} \in [\frac{x_{left}+x_{right}}{2}, x_{right}]. \end{cases} \quad (3.3)$$

<sup>236</sup> For example, Figure 3.1 shows the derivative SRV filters with  $k = 2$  for the first and second derivatives at the left boundary.

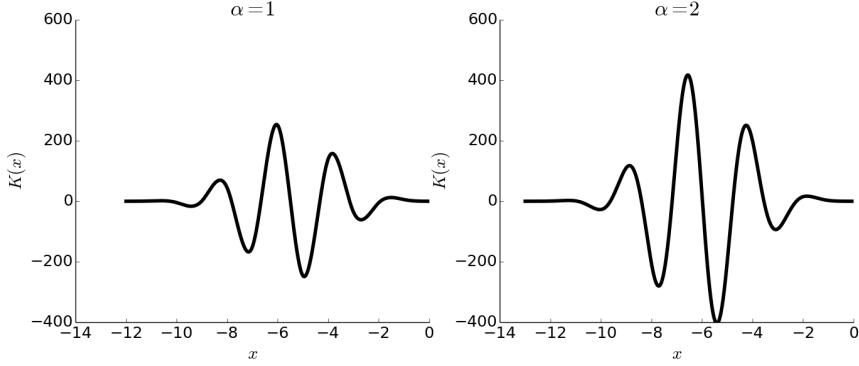


Figure 3.1: The derivative SRV filters (first and second derivatives) before convolution at the left boundary with  $k = 2$  and scaling  $H = 1$ . The boundary is represented by  $x = 0$ .

<sup>237</sup>

<sup>238</sup> **Remark 3.2.** The theoretical analysis of the derivative SRV filter remains the same as Theorem 3.3  
<sup>239</sup> with  $r = 4k$ . The difference between the derivative SRV filter and the symmetric derivative filter is the  
<sup>240</sup> scaling  $H = h^\mu$ . The scaling of the derivative SRV filter is  $H = h^{\frac{2k+1}{5k+2+\alpha}}$ , which is much larger than the  
<sup>241</sup> scaling of the symmetric derivative filter,  $H = h^{\frac{2k+1}{3k+2+\alpha}}$ .

### <sup>242</sup> 3.2.2. Derivative RLKV Filter

<sup>243</sup> For the RLKV filter, we need to shift the  $2k + 1$  central B-splines and then change the extra general  
<sup>244</sup> B-spline according to the derivative order  $\alpha$ . To complete these changes, we have to change the knot  
<sup>245</sup> sequence (2.10), which is used only for the DG approximation  $u_h$  without derivatives. For the derivative  
<sup>246</sup> RLKV filter near the left boundary (similar for the right boundary), we need to redistribute the knots  
<sup>247</sup> in the knot matrix  $\mathbf{T}$  to meet the derivative requirement by

$$T(\gamma, j) = \begin{cases} -3k - 1 - \alpha + j + \gamma + \frac{\bar{x} - x_{left}}{h}, & 0 \leq \gamma \leq 2k, 0 \leq j \leq k + 1 + \alpha; \\ \frac{\bar{x} - x_{left}}{h} + \min\{j - \alpha, 0\}, & \gamma = 2k + 1, 0 \leq j \leq k + 1 + \alpha, \end{cases} \quad (3.4)$$

<sup>248</sup> and the position-dependent derivative filter is given by

$$K_{\mathbf{T}}^{(2k+2, k+1+\alpha)}(x) = \underbrace{\sum_{\gamma=0}^{2k} c_\gamma^{(2k+2, k+1)} \psi_{\mathbf{T}(\gamma)}^{(k+1+\alpha)}(x)}_{\text{Position-dependent filter with } 2k + 1 \text{ central B-splines}} + \underbrace{c_{2k+1}^{(2k+2, k+1+\alpha)} \psi_{\mathbf{T}(2k+1)}^{(k+1+\alpha)}}_{\text{General B-spline}}, \quad (3.5)$$

<sup>249</sup> **Remark 3.3.** It is necessary to use a B-spline of order  $k + 1 + \alpha$  instead of  $k + 1$  when  $\alpha > k$ . In formula  
<sup>250</sup> (3.5), if we keep the order of B-spline as  $k + 1$ , when  $\alpha > k$  the knot sequence  $\mathbf{T}(2k + 1)$  becomes a  
<sup>251</sup> uniformly spaced knot sequence, and then the general B-spline  $\psi_{\mathbf{T}(2k+1)}^{(k+1+\alpha)}$  added at the boundary reduces  
<sup>252</sup> to a central B-spline. Then, the purpose of adding a special B-spline at the boundary fails, and this  
<sup>253</sup> special B-spline is needed to place more weights on the filtered points.

254 We note that the derivative RLKV filter allows us to approximate arbitrary order of derivatives near  
 255 boundaries theoretically. For example, Figure 3.2 shows the derivative RLKV filters with  $k = 2$  for the  
 256 first and second derivatives at the left boundary. Compared to the derivative SRV filter in Figure 3.1,  
 257 the derivative RLKV filter clearly has reduced support and magnitude (range from  $-400$  to  $600$  versus  
 258  $-4$  to  $6$ ).

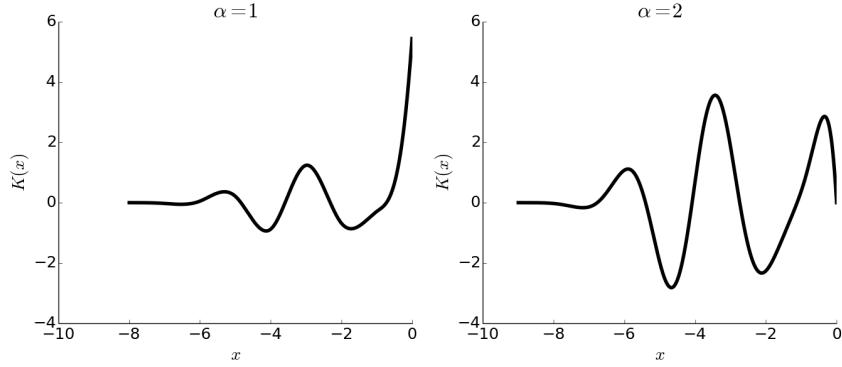


Figure 3.2: The derivative RLKV filters (first and second derivatives) before convolution at the left boundary with  $k = 2$  and scaling  $H = 1$ . The boundary is represented by  $x = 0$ .

258  
 259 **Theorem 3.4.** Under the same conditions as in Lemma 3.2, let  $K_{HT}^{(2k+2,k+1+\alpha)}$  be the derivative RLKV  
 260 filter (3.5). We have

$$\left\| \partial_x^\alpha u - \partial_x^\alpha \left( K_{HT}^{(2k+2,k+1+\alpha)} \star u_h \right) \right\|_{0,\Omega_0} \leq Ch^{\mu(2k+2)},$$

261 where  $H = h^\mu$ ,  $\mu = \frac{2k+1}{3k+3+\alpha}$ .

*Proof.*

$$\begin{aligned} & \left\| \partial_x^\alpha u - \partial_x^\alpha \left( K_{HT}^{(2k+2,k+1+\alpha)} \star u_h \right) \right\|_{0,\Omega_0} \\ & \leq C_0 H^{2k+2} + \left\| \partial_x^\alpha \left( \sum_{\gamma=0}^{2k} c_\gamma \psi_{HT(\gamma)}^{(k+1+\alpha)} \star (u - u_h) \right) \right\|_{0,\Omega_0} + \left\| \partial_x^\alpha \left( c_{2k+1} \psi_{HT(2k+1)}^{(k+1+\alpha)} \star (u - u_h) \right) \right\|_{0,\Omega_0} \end{aligned}$$

262 For the second term on the left side of the above inequality, which only involves central B-splines, similar  
 263 to Theorem 3.3, we have

$$\left\| \partial_x^\alpha \left( \sum_{\gamma=0}^{2k} c_\gamma \psi_{HT(\gamma)}^{(k+1+\alpha)} \star (u - u_h) \right) \right\|_{0,\Omega_0} \leq C_1 h^{2k+1} H^{-(k+1+\alpha)}.$$

For the third term with a general B-spline, we have

$$\begin{aligned} \left\| \partial_x^\alpha \left( c_{2k+1} \psi_{HT(2k+1)}^{(k+1+\alpha)} \star (u - u_h) \right) \right\|_{0,\Omega_0} & \leq C_2 \sum_{\beta \leq k+1} \left\| c_{2k+1} \left( \frac{d^{\alpha+\beta}}{dx^{\alpha+\beta}} \psi_{HT(2k+1)}^{(k+1)} \right) \star (u - u_h) \right\|_{-(k+1),\Omega_{1/2}} \\ & \leq C_2 \sum_{\beta \leq k+1} \left\| c_{2k+1} \left( \frac{d^{\alpha+\beta}}{dx^{\alpha+\beta}} \psi_{HT(2k+1)}^{(k+1)} \right) \right\|_{L^1} \|u - u_h\|_{-(k+1),\Omega_1} \\ & \leq C_3 \sum_{\beta \leq k+1} H^{-(\alpha+\beta)} \left\| \left( \frac{d^{\alpha+\beta}}{dx^{\alpha+\beta}} \psi_{HT(2k+1)}^{(k+1)} \right) \right\|_{L^1} \|u - u_h\|_{-(k+1),\Omega_1} \end{aligned}$$

$$\leq C_4 h^{2k+1} H^{-(k+1+\alpha)},$$

264 where

$$\Omega_0 + \text{supp}(K_{H\mathbf{T}}^{(2k+2,k+1+\alpha)}) \subset \Omega_{1/2}, \quad \text{and} \quad \Omega_{1/2} + \text{supp}(K_{H\mathbf{T}}^{(2k+2,k+1+\alpha)}) \subset \Omega_1.$$

265 Then, we have

$$\left\| \partial_x^\alpha u - \partial_x^\alpha \left( K_{H\mathbf{T}}^{(2k+2,k+1+\alpha)} \star u_h \right) \right\|_{0,\Omega_0} \leq C_0 H^{2k+2} + C_5 h^{2k+1} H^{-(k+1+\alpha)}.$$

266 Similar to the symmetric filter case in Theorem 3.3, we require the scaling  $H$  satisfies  $H^{2k+2} =$   
267  $h^{2k+1} H^{-(k+1+\alpha)}$  and finally, we have

$$\left\| \partial_x^\alpha u - \partial_x^\alpha \left( K_{H\mathbf{T}}^{(2k+2,k+1+\alpha)} \star u_h \right) \right\|_{0,\Omega_0} \leq C h^{\mu(2k+2)},$$

268 where  $H = h^\mu$  and  $\mu = \frac{2k+1}{3k+3+\alpha}$ . □

269 **Remark 3.4** (Discussion of Support Size of the Filters). Theorem 3.3 and Theorem 3.4 give convergence  
270 rates of the symmetric and position-dependent derivative filters, respectively. One can easily verify that  
271 the convergence rates are better than calculating the derivatives of DG approximation directly,  $k+1-\alpha$ .  
272 For the scaling  $H = h^\mu$ , for convenience we let the degree  $k \rightarrow \infty$ , then the symmetric derivative filter  
273 and derivative RLKV filters have the scaling  $H = h^{2/3}$  and the derivative SRV filter has the scaling  
274  $H = h^{2/5}$ . In order to show the difference of support size of the different filters, we present Figure 3.3  
to show a direct comparison. From Figure 3.3, we can see that the SRV filter requires a much larger

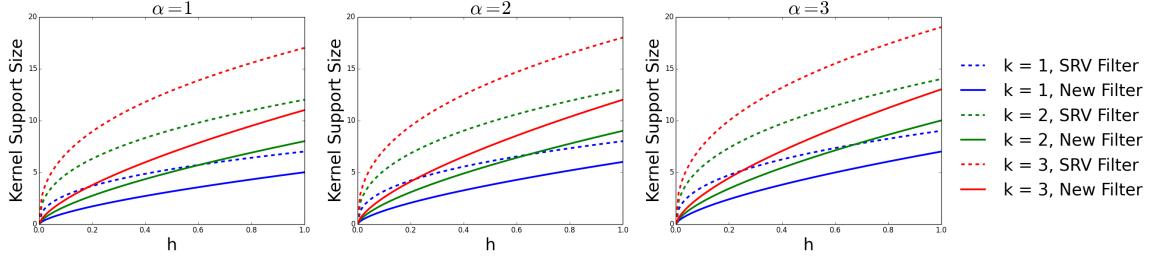


Figure 3.3: Comparison of support sizes of the derivative SRV filter and the derivative RLKV filters. The symmetric derivative filter has the same support size as the derivative RLKV filter.

275 support size than the RLKV filter. The large support size usually will lead to computational problems  
276 (increased flop counts, round-off error, etc.).

277 However, we notice that the scaling  $H = h^\mu$  is still quite large compared to  $h$ . The large support  
278 usually has negative effects on the accuracy over coarse meshes. Let the domain be  $\Omega = [0, 1]$  and  
279  $h = 1/N$ , where  $N$  is the number of elements. In order to guarantee the conclusions in Theorem 3.3 and  
280 Theorem 3.4, we must choose  $N$  large enough so that the support size of filters is less than the domain  
281 size, which requires

$$(r + k + \alpha + 1)h^\mu \leq 1 \implies N \geq (r + k + \alpha + 1)^{1/\mu},$$

283 here  $r = 2k$  for the symmetric and derivative RLKV filters and  $r = 4k$  for the derivative SRV filter.  
284 Table 3.1 gives the minimum number of elements for different filters. We note that for the SRV filter, the  
285 required number of elements is always too large, this is one important reason that the SRV filter performs  
286 poorly over nonuniform meshes in the numerical examples. Once  $N$  is smaller than the minimum  
287 requirement given in Table 3.1, we have to rescale the filter by using scaling  $H = 1/(r + k + \alpha + 1)$ .  
288 However, this rescaling technique normally has negative effects on the accuracy order. There are two  
289 ways by which to overcome these drawbacks. One is to keep the order of B-splines as  $k+1$  as the

Table 3.1: The minimum requirement of element number  $N$  according to the derivative order  $\alpha$ . Here,  $N_1$  is used for the symmetric and derivative RLKV filters and  $N_2$  is used for the derivative SRV filter.

| $N_1 \backslash N_2$ | $\alpha = 0$ | $\alpha = 1$ | $\alpha = 2$ | $\alpha = 3$ | $\alpha = 4$ | $\alpha = 5$ |
|----------------------|--------------|--------------|--------------|--------------|--------------|--------------|
| $k = 1$              | 8<br>89      | 12<br>130    | 15<br>182    | 19<br>243    | 23<br>317    | 27<br>402    |
| $k = 2$              | 19<br>402    | 23<br>499    | 27<br>610    | 32<br>734    | 37<br>872    | 42<br>1024   |
| $k = 3$              | 32<br>1024   | 37<br>1192   | 42<br>1375   | 47<br>1574   | 53<br>1789   | 59<br>2021   |

290 nonderivative filter and then calculate the derivatives directly as mentioned in [9]. This method can  
291 decrease the support size of the filters from  $(r+k+\alpha+1)H$  to  $(r+k+1)H$ . In the next section, we will  
292 present a numerical comparison of using the order of B-splines of  $k+1$  and  $k+1+\alpha$ . The other way  
293 will be presented in our future work; it will give an alternative version of Lemma 3.2 according to the  
294 given nonuniform mesh. It allows us to choose a smaller scaling  $H$  (or larger  $\mu$ ) than that in Theorems  
295 3.3 and 3.4.

#### 296 4. Numerical Results

297 In the previous section, we proposed two position-dependent derivative filters and investigated how  
298 to choose the proper scaling of the filters over nonuniform meshes. We also proved that the filtered  
299 solutions have better accuracy order and smoothness compared to the original DG approximations  
300 regardless of the derivative order  $\alpha$ . We now turn to the numerical examples of the position-dependent  
301 derivative filtering. The aims of this section are:

- 302 1. Testing the position-dependent derivative filters (the SRV and RLKV filter) for uniform meshes,  
303 which has never been done before;  
304 2. Applying the symmetric and position-dependent derivative filters over different nonuniform meshes;  
305 3. Comparing the derivative filters with different order B-splines. In order of convenience, we denote  
306 the following two notation:  
307     • the derivative of the filtered solution,  $\partial_x^\alpha u_h^*$ . This filtered solution using the standard filter  
308 and then takes the derivative.  
309     • the filtered derivative,  $(\partial_H^\alpha \tilde{K}_H) \star u_h$ , which uses the higher order derivative filter  $K_H^{(r+1,k+1+\alpha)}$   
310 for filtering the DG solution.

311 We note that the DG approximation makes sense only when  $\alpha \leq k$ . In addition, the derivative of the  
312 filtered solution  $\partial_x^\alpha u_h^*$  loses the wanted accuracy order when  $\alpha > k$  ( $u_h^* = K_H^{r+1,k+1} \star u_h$  is a  $C^{k-1}$   
313 function only). Therefore, we mainly present comparison examples with  $\alpha \leq k$  situation in this section.  
314 When  $\alpha > k$ , we only present the results of the filtered derivative  $(\partial_H^\alpha \tilde{K}_H) \star u_h$ , and we point out  
315 that the filtered solution  $(\partial_H^\alpha \tilde{K}_H) \star u_h$  has a theoretical meaning for an arbitrary  $\alpha$ , but the accuracy  
316 deteriorates with each successive derivative. However, we also note that once  $\alpha > k$ , the nonuniform  
317 meshes have to be sufficiently refined in order to see the accuracy improvement. Because of these  
318 reasons, we only present  $\alpha = k+1$  case for nonuniform meshes. Also, since the symmetric derivative  
319 filter is applied in the interior region of each example, we do not present it separately.

320 **Remark 4.1.** For the following numerical examples:

- 321     • when the number of elements is less than the minimum requirement in Table 3.1, a rescaling  
322 technique is used;

- 323     • quadruple precision is used for the SRV filter, and double precision is used for the RLKV filter  
 324       and all two-dimensional examples;  
 325     • the blending function  $\theta(x)$  in (2.8) is no longer needed for the RLKV filter (see [8]), therefore the  
 326       function  $\theta(x)$  is not used in the following examples.

327     4.1. Uniform Mesh

328     Before approaching nonuniform meshes, we first apply the position-dependent derivative filters over  
 329     uniform meshes. Here we present results of using both the SRV filter and the RLKV filter since each  
 330     of them has its advantages over uniform meshes that we address in the following examples. Consider a  
 331     linear convection equation

$$u_t + u_x = 0, \quad x \in [0, 1], \quad (4.1)$$

$$u(x, 0) = \sin(2\pi x),$$

332     at time  $T = 1$  with periodic boundary conditions. For uniform meshes, we can also use scaling  $H = h^\mu$   
 333     and obtain results as Theorems 3.3 and 3.4 described. However, according to the analysis in [3, 8, 10],  
 334     in order to maximize the benefits of using central B-splines over uniform meshes, we choose the uniform  
 335     mesh size,  $h$ , as the filter scaling. Here, we compare the derivatives of the DG approximation, the  
 336     filtered solutions (the SRV and RLKV filter) with using B-splines of order  $k + 1 + \alpha$  (Table 4.1 and  
 337     Figure 4.1) and using B-splines of order  $k + 1$  (Table 4.2 and Figure 4.2). From the tables, we can see  
 338     that the filtered solutions  $(\partial_H^\alpha \tilde{K}_H) \star u_h$  and  $\partial_x^\alpha u_h^*$  have better accuracy compared to the original DG  
 339     solutions.

340     With the scaling  $H = h$ , the SRV filter clearly has an advantage for uniform meshes. Because the  
 341     SRV is constructed using only central B-splines, and was proved to have  $2k+1$  accuracy order regardless  
 342     of the derivative order  $\alpha$  for linear equations over uniform meshes in [9]. In Tables 4.1 and 4.2, the SRV  
 343     filter shows much better accuracy compared to the RLKV filter near the boundaries, especially when  
 344      $\alpha$  is large. For the RLKV position-dependent derivative filter, we notice that the filtered solutions only  
 345     have accuracy of order  $k + 1 - \alpha$  in Tables 4.1 and 4.2. This is because we use scaling  $H = h$  instead of  
 346     scaling  $H = h^\mu$  in Theorem 3.4. We note that if using a multi-precision package is acceptable, then the  
 347     SRV filter is more advantageous for the accuracy order. However, if only double precision is available  
 348     during computation (for example, GPU computing), then in order to avoid the round-off error, the  
 349     RLKV filter is a better choice, see [8]. However, when  $\alpha > k$ , the optimal choice is still the SRV filter  
 350     with B-splines of order  $k + 1 + \alpha$  because only this filter does not lose the accuracy with each successive  
 351     derivative.

352     We note that the derivative of filtered solution  $\partial_x^\alpha u_h^*$  also performs well near boundaries for uniform  
 353     meshes. However, for the derivative order  $\alpha > k$ , we still need to use higher-order B-splines to construct  
 354     the derivative filters. Figures 4.1 and 4.2 present the point-wise error plots in log scale using the DG  
 355     approximation of degree  $k = 2$ . After filtering, the filtered approximations are much smoother than the  
 356     DG solution, but in order to reduce oscillations in the interior regions, we still have to use B-splines of  
 357     order  $k + 1 + \alpha$ .

358     **Remark 4.2.** For uniform meshes, we choose to use the scaling  $H = h$  instead of the scaling  $H = h^\mu$   
 359     in Theorem 3.3. This is because for uniform meshes, the scaling  $H = h$  can provide a better accuracy  
 360     order of  $2k + 1$  compared to the conclusion in Theorem 3.3, especially in the interior region. Also, the  
 361     SRV filter benefits of the scaling  $H = h$  in the boundary region once quadruple precision is used. If the  
 362     scaling  $H = h^\mu$  is used for uniform meshes, the accuracy order will decrease and the error magnitude  
 363     will increase in the interior region. However, the RLKV filter will have better accuracy order in the  
 364     boundary region, and the error magnitude will improve once the mesh is sufficiently refined.

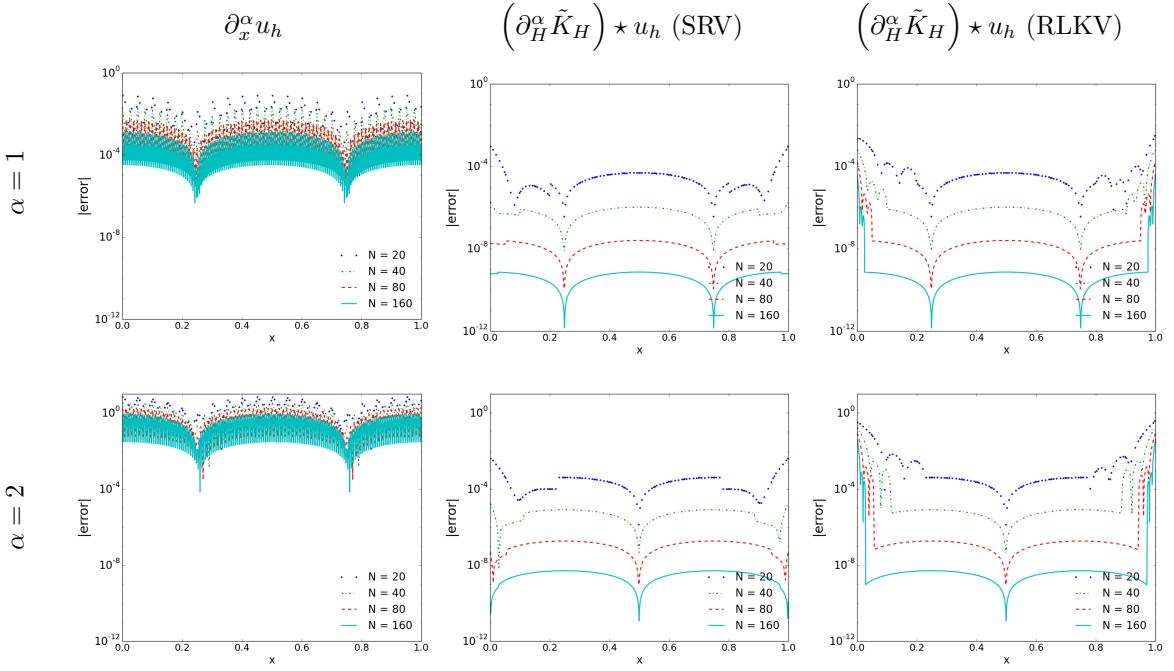


Figure 4.1: Comparison of the point-wise errors in log scale of the first and second derivatives of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions (the SRV and RLKV filters) for linear convection equation (4.1), over uniform meshes. The B-spline order is  $k + 1 + \alpha$ , the filter scaling is taken as  $H = h$ , and  $k = 2$ .

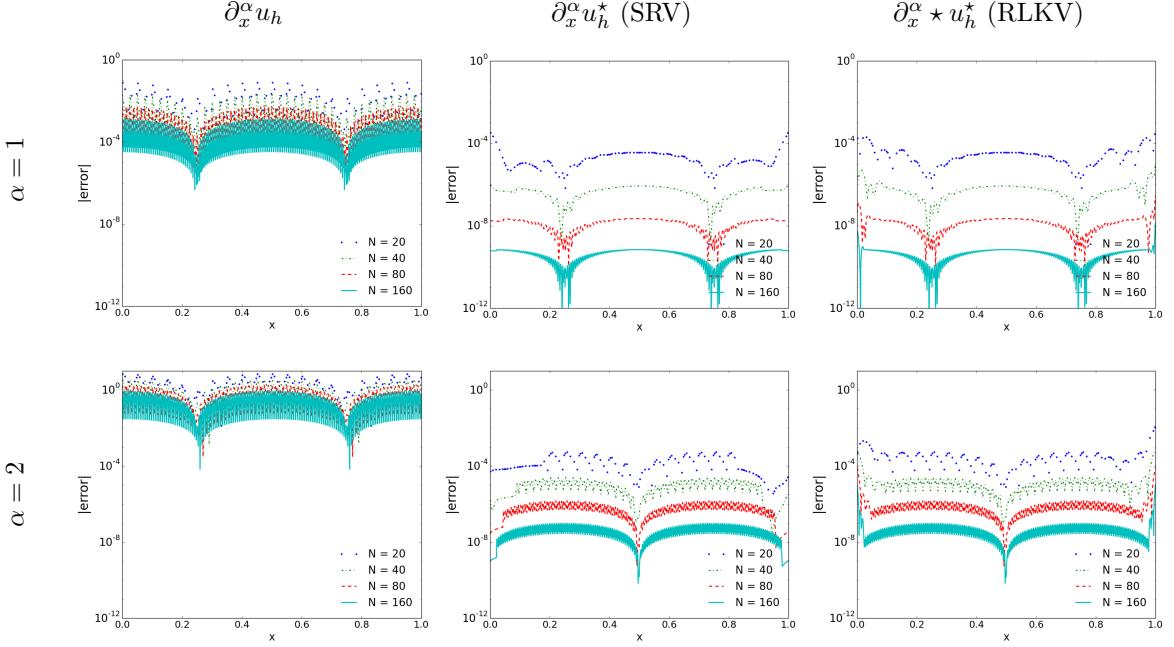


Figure 4.2: Comparison of the point-wise errors in log scale of the first derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions (the SRV and RLKV filters) for linear convection equation (4.1), over uniform meshes. The B-spline order is  $k + 1$ , the filter scaling is taken as  $H = h$ , and  $k = 2$ .

365    4.1.1. *Smoothly-Varying Mesh*

366    As mentioned in [6, 8], there is a particular family of nonuniform meshes, smoothly-varying meshes.  
 367    In [8], the authors proved that the filtered solutions (both the SRV and RLKV filters) have the similar  
 368    performance over smoothly-varying meshes compared to uniform meshes. However, it would be of  
 369    practical interests to show the performance of the position-dependent derivative filters over smoothly-  
 370    varying meshes, especially for smoothly increasing/decreasing meshes.

371    Consider a linear convection equation with Dirichlet boundary conditions

$$\begin{aligned} u_t + u_x &= 0, \quad x \in [0, 1], \\ u(x, 0) &= \sin(2\pi x), \\ u(0, t) &= \sin(-2\pi t), \end{aligned} \tag{4.2}$$

372    at time  $T = 1$  over a smoothly decreasing mesh defined in [8]:

$$x = \xi - 0.2(\xi - 1)\xi,$$

373    where  $x$  is the smoothly decreasing mesh variable and  $\xi$  is the variable of the uniform mesh over domain  
 374     $[0, 1]$ .

375    Similar to the uniform mesh case, we choose the local mesh size as the filter scaling,  $H = \Delta x_j$   
 376    according to [8]. Here, in order to save space, we present results for the filtered derivative  $(\partial_H^\alpha \tilde{K}_H) \star u_h$   
 377    only. The  $L^2$  and  $L^\infty$  errors are presented in Table 4.3 with the first three derivatives over the above  
 378    smoothly decreasing mesh. The respective point-wise error plots ( $k = 2$  case) are given in Figure 4.3.  
 379    Here, we only point out one phenomenon that is very different to the uniform mesh case. The RLKV  
 380    filter provides better accuracy compared to the SRV filter near the boundaries, see Table 4.3. However,  
 381    both the SRV and RLKV filters can improve the accuracy of the original DG solutions once the mesh  
 382    is sufficiently refined.

383    4.2. *Nonuniform Mesh*

384    Now we show the main results of this paper: the position-dependent derivative filtering over arbitrary  
 385    nonuniform meshes. Before proceeding further, we first give the numerical setting of nonuniform meshes.  
 386    In order to generate a more general format for nonuniform meshes, we use a random number generator  
 387    to design the following two meshes.

388    **Mesh 4.3.** The first nonuniform mesh that we consider is defined by

$$x_{\frac{1}{2}} = 0, \quad x_{N+\frac{1}{2}} = 1, \quad x_{j+\frac{1}{2}} = \left(j + b \cdot r_{j+\frac{1}{2}}\right) h, \quad j = 1, \dots, N - 1$$

389    where  $\left\{r_{j+\frac{1}{2}}\right\}_{j=1}^{N-1}$  are random numbers between  $(-1, 1)$ , and  $b \in (0, 0.5]$  is a constant number. The size  
 390    of element  $\Delta x_j = x_{j+\frac{1}{2}} - x_{j-\frac{1}{2}}$  is between  $((1 - 2b)h, (1 + 2b)h)$ . In order to save space, in this paper  
 391    we present an example with  $b = 0.4$  only, other values of  $b$  such as 0.1, 0.2 and 0.45 had been calculated  
 392    also.

393    **Mesh 4.4.** The second nonuniform mesh is more irregular than the first one. We distribute the element  
 394    interface by  $x_{j+\frac{1}{2}}$ ,  $j = 1, \dots, N - 1$  randomly for the entire domain and require only

$$\Delta x_j = x_{j+\frac{1}{2}} - x_{j-\frac{1}{2}} \geq b \cdot h, \quad j = 0, \dots, N.$$

395    In this paper, we only present  $b = 0.5$  case for this mesh, other values of  $b$  such as 0.6, 0.8, etc. had  
 396    been calculated also.

397    We remark that we have tested various differential equations over both kinds of nonuniform meshes:  
 398    Mesh 4.3 and Mesh 4.4. However, the filtered approximations have similar performances since the  
 399    performance mainly depends on the mesh. In order to save space, we choose to present one equation  
 400    for each nonuniform mesh.

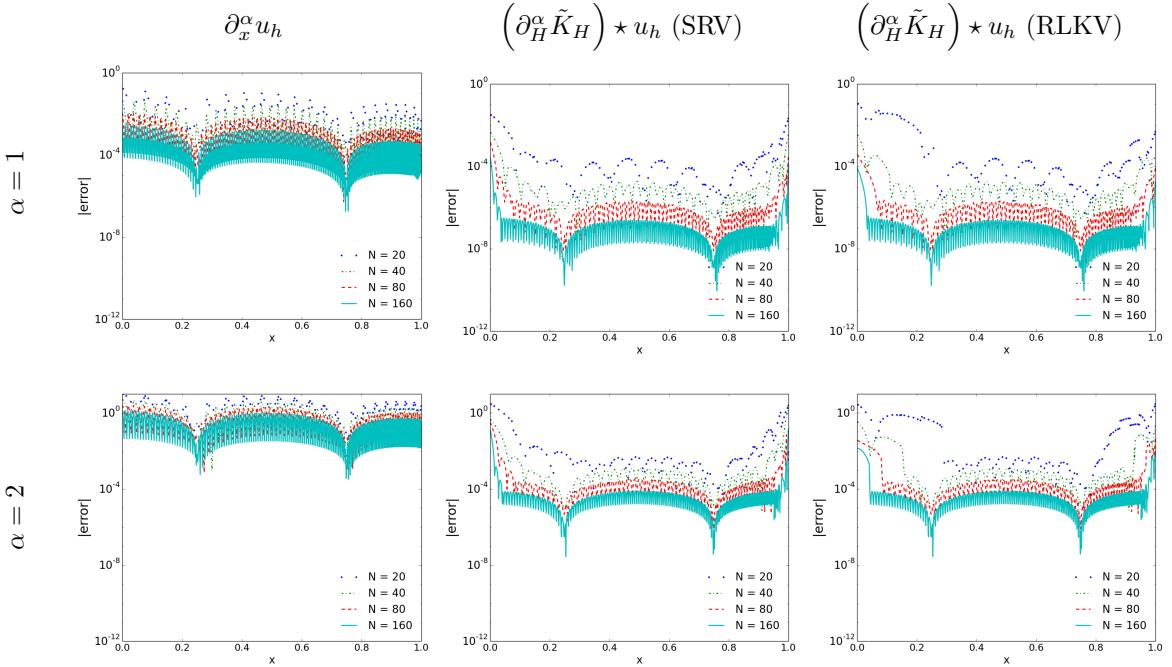


Figure 4.3: Comparison of the point-wise errors in log scale of the first and second derivatives of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions (the SRV and RLVK filters) for the Dirichlet (4.2), over smoothly decreasing meshes. The B-spline order is  $k + 1 + \alpha$ , the filter scaling is taken as  $H = \Delta x_j$ , and  $k = 2$ .

#### 401 4.2.1. Comparison of the SRV filter and RLVK filter over Nonuniform Mesh

402 In [8], the authors showed that the SRV filter has worse performance compared to the RLVK filter  
 403 over nonuniform meshes for filtering the solution itself. We also mentioned that the enormous support  
 404 size of the SRV filter causes problems: we have to rescale the SRV filter to fit the domain size then we can  
 405 not guarantee neither the accuracy order nor error reduction. Table 3.1 shows the minimum requirement  
 406 of the number of elements for the SRV filter, and we can see that it is difficult to satisfy. Based on  
 407 these deficiencies, we conclude that the SRV filter is not suitable for approximating derivatives over  
 408 nonuniform meshes. However, in order to provide a complete view of the position-dependent derivative  
 409 filters, we still give one example of using the SRV filter for the first derivative over Mesh 4.3. Table  
 410 4.4 shows that with the SRV filter, the filtered solutions (no matter what order of B-splines is used)  
 411 are even worse the derivative of DG approximations. In the rest of this section, we focus on testing the  
 412 RLVK filter over nonuniform meshes.

#### 413 4.2.2. Linear Equation over Mesh 4.3

414 For Mesh 4.3, we present results for the linear convection equation (4.1) with the first, second and  
 415 third derivatives. The  $L^2$  and  $L^\infty$  norm errors are given in Table 4.5 and Figure 4.4 shows the point-wise  
 416 error in log scale. When  $\alpha \leq k$ , both the derivative of filtered solution  $\partial_x^\alpha u_h^*$  and the filtered derivative  
 417  $(\partial_H^\alpha \tilde{K}_H) * u_h$  have better accuracy and convergence rates than the original DG approximation. The  
 418 filtered derivative  $(\partial_H^\alpha \tilde{K}_H) * u_h$  shows better smoothness and theoretically has a better accuracy  
 419 order than the derivative of the filtered solution  $\partial_x^\alpha u_h^*$  when  $\alpha \leq k$ , but  $\partial_x^\alpha u_h^*$  has better accuracy near  
 420 the boundaries. For smoothness, the results are similar to the uniform mesh case;  $(\partial_H^\alpha \tilde{K}_H) * u_h$  has  
 421 fewer oscillations compared to the DG solution and  $\partial_x^\alpha u_h^*$ . Furthermore, we point out that by using  
 422 higher-order B-splines we can disregard the requirement that  $\alpha \leq k$ .

423 The point-wise error plots given in Figure 4.4, the middle column is the filtered approximation

424  $\partial_x^\alpha u_h^*$ , which shows more oscillations than the  $(\partial_H^\alpha \tilde{K}_H) * u_h$ , especially in the interior regions. We note,  
 425 however that the support size of the filter that uses a higher-order B-spline increases with the derivative  
 426 order  $\alpha$  and it slightly increases the computational cost. Near the boundaries, the filtered solutions  
 427 have a larger error magnitude than those in the interior region. Because near the boundaries we cannot  
 428 obtain symmetric information around the filtered points, and the general B-spline has less regularity  
 429 compared to the central B-spline. We note that the coarse meshes (such as  $N = 20$  or even  $N = 40$ )  
 430 are not sufficient to use the position-dependent derivative filter, the filtered solution may have worse  
 431 accuracy compared to the original DG approximation.

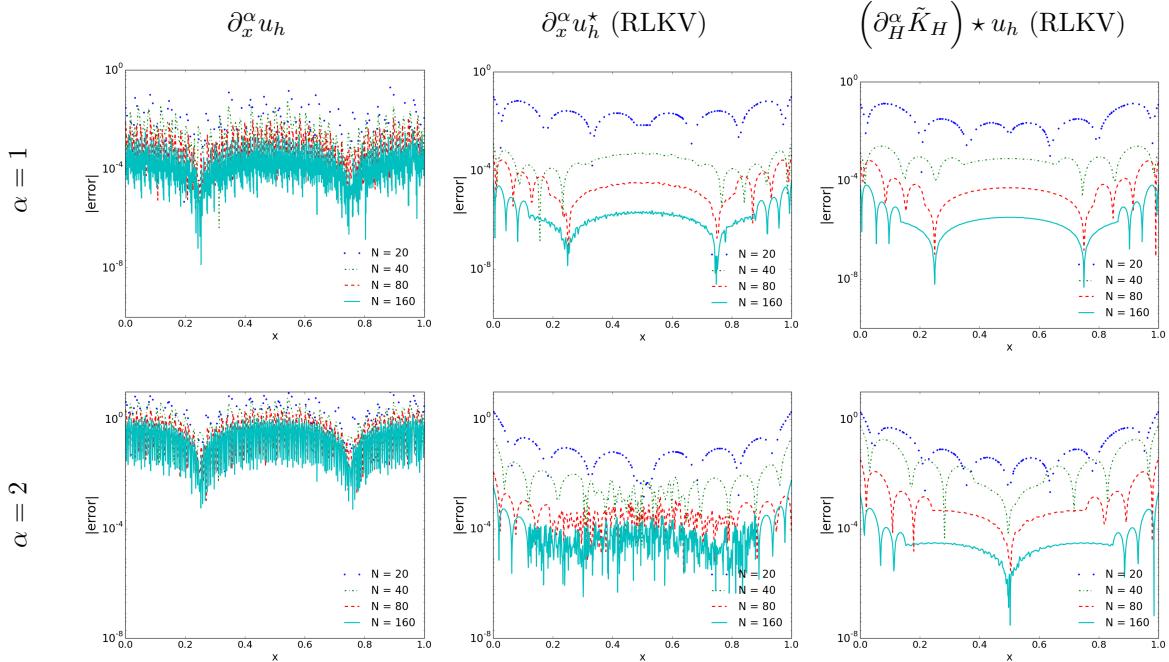


Figure 4.4: Comparison of the point-wise errors in log scale of the first and second derivatives of DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions  $\partial_x^\alpha u_h^*$  and  $(\partial_H^\alpha \tilde{K}_H) * u_h$  (with the RLKV filter) for linear convection equation (4.1) over Mesh 4.3. The filter scaling is taken as  $H = h^{2/3}$ , and  $k = 2$ .

#### 432 4.2.3. Variable Coefficient Equation over Mesh 4.4

433 After testing the linear convection equation (4.1), we move to a variable coefficient equation with  
 434 periodic boundary conditions,

$$\begin{aligned}
 u_t + (au)_x &= f, \quad (x, t) \in [0, 1] \times (0, T) \\
 u(x, 0) &= \sin(2\pi x),
 \end{aligned} \tag{4.3}$$

435 where the variable coefficient  $a(x, t) = 2 + \sin(2\pi(x + t))$  and the right side term  $f(x, t)$  are chosen to  
 436 make the exact solution be

$$u(x, t) = \sin(2\pi(x - t)).$$

437 As with the linear convection example, we present the  $L^2$  and  $L^\infty$  errors in Table 4.6 with the first  
 438 three derivatives over Mesh 4.4. The respective point-wise error plots ( $k = 2$  case) are shown in Figure  
 439 4.5. The results are similar to the results for the constant coefficient case. In order to save space we no  
 440 longer repeat the descriptions, which are similar. However, we still want to point out one phenomenon.

441 In this variable coefficient case, the filtered solution  $\partial_x^\alpha u_h^*$  shows somewhat better accuracy than the  
442 filtered solution  $(\partial_H^\alpha \tilde{K}_H) * u_h$  near the boundaries when  $\alpha \leq k$ . This performance suggests that when  
443  $\alpha \leq k$  we can consider not increasing the order of the B-splines, although it causes more oscillations in  
444 the error.

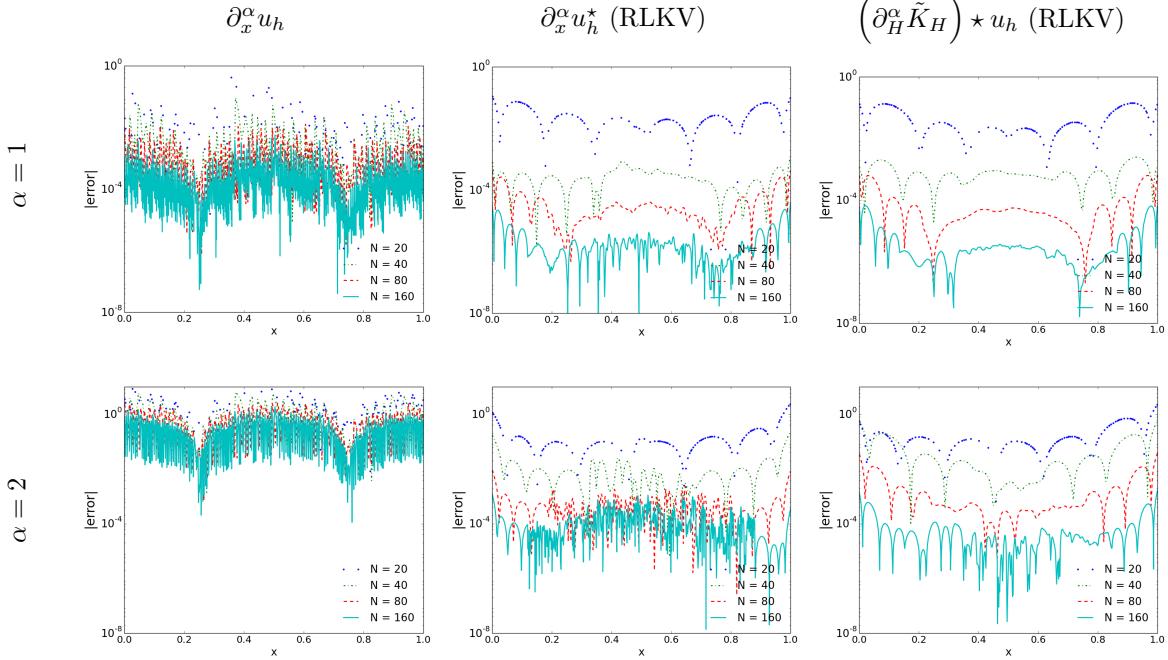


Figure 4.5: Comparison of the point-wise errors in log scale of the first and second derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions  $\partial_x^\alpha u_h^*$  and  $(\partial_H^\alpha \tilde{K}_H) * u_h$  (with the RLKV filter) for variable coefficient equation (4.3) over Mesh 4.4. The filter scaling is taken as  $H = h^{2/3}$ , and  $k = 2$ .

445 **Remark 4.5.** Here we conclude the consequences of using B-splines of order  $k + 1$  compared to using  
446 normal order  $k + 1 + \alpha$ ; they are the following:

- 447 • it can give better accuracy near the boundaries;
- 448 • it can give better accuracy in the interior regions (when  $\alpha \ll k$ ), but it damages the smoothness  
449 of filtered solution (more oscillations);
- 450 • it has a smaller support size;
- 451 • it allows the use of the symmetric filter over a larger area; and
- 452 • it requires  $\alpha \leq k$ .

## 453 5. Two-Dimensional Example

For the two-dimensional example, we consider a 2D version of the linear convection equation

$$\begin{aligned} u_t + u_x + u_y &= 0, & (x, y) \in [0, 1] \times [0, 1], \\ u(x, y, 0) &= \sin(2\pi x + 2\pi y), \end{aligned} \tag{5.1}$$

454 at time  $T = 1$  with periodic boundary conditions. The nonuniform meshes we used are the 2D quadrilateral extension of Meshes 4.3 and 4.4. Here, we show the cross-derivative  $\partial_{xy}^2$ , the first derivatives  $\partial_x$  and  $\partial_y$  are omitted as they are similar to the 1D results. We give the  $L^2$  and  $L^\infty$  error in Tables 5.1 -  
455 5.2 and the point-wise error plots in Figures 5.1 - 5.2. We note that the filtered accuracy error seems  
456 slightly worse than the DG approximation over coarse meshes, because near the boundary regions we  
457 need sufficiently refined meshes to show the advantage of the position-dependent filter. Once the mesh  
458 is sufficient refined, we see better results. We also note that although we require a relatively refined  
459 mesh for boundary regions, the results in the interior regions are always much better (see the point-wise  
460 error plots).  
461

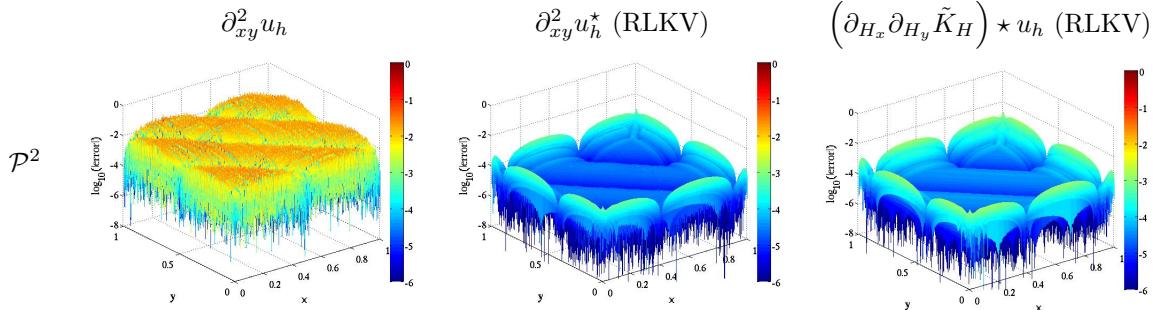


Figure 5.1: Comparison of the point-wise errors in log scale of the cross-derivative DG approximation  $\partial_{xy}^2 u_h$  together with the filtered solutions for the two-dimensional linear advection equation (5.1) over Mesh 4.3 (2D,  $N = 160 \times 160$ ).

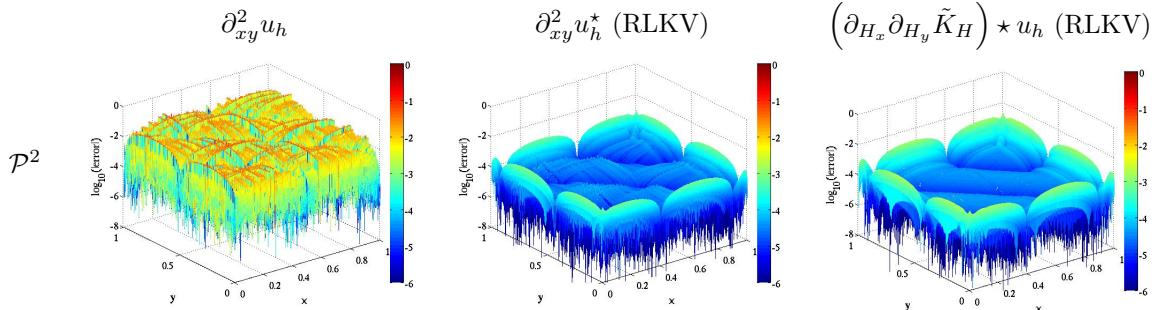


Figure 5.2: Comparison of the point-wise errors in log scale of the cross-derivative DG approximation  $\partial_{xy}^2 u_h$  together with the filtered solutions for the two-dimensional linear advection equation (5.1) over Mesh 4.4 (2D,  $N = 160 \times 160$ ).

## 463 6. Conclusion

464 In this paper, we have proposed two position-dependent derivative filters (the SRV and RLKV filter),  
465 to approximate the derivatives of the discontinuous Galerkin solutions over uniform and nonuniform  
466 meshes. These position-dependent derivative filters allow us to obtain more accurate derivatives of the  
467 DG solutions compared to calculating the derivatives of DG solutions directly. The derivative SRV  
468 filter uses  $4k + 1$  central B-splines, and obtains a convergence rate of  $2k + 1$  over uniform meshes  
469 regardless of derivative order. The derivative RLKV filter uses  $2k + 1$  central B-splines and an extra  
470 general B-spline, where the general B-spline relies on the derivative order  $\alpha$ . We have proved that the  
471 derivative RLKV filter has accuracy order of  $\mu(2k + 2)$  when using a filter scaling  $H = h^\mu$  ( $\mu \approx 2/3$ ).  
472 Additionally, we are able, for the first time, to extend the symmetric derivative filter to nonuniform  
473 meshes. Through numerical examples, we compared the derivative SRV and RLKV filter over uniform  
474 and nonuniform meshes. We demonstrated that once the required conditions are satisfied the derivative  
475 SRV filter has a better performance over uniform meshes compared to the derivative RLKV filter.

476 However, for nonuniform meshes, only the derivative RLKV filter can maintain its performance and  
477 improve the accuracy of the DG approximations. Also, we compared derivative filters with different  
478 order of B-splines: order  $k + 1$  and order  $k + 1 + \alpha$ . Numerical results indicate that using B-splines of  
479 order  $k + 1$  may improve the accuracy of the filtered solution near the boundaries. For interior regions  
480 where the symmetric derivative filtering is applied, using B-splines of order  $k + 1 + \alpha$  shows better  
481 accuracy and smoothness. Lastly, we point out that for given nonuniform meshes there may exist a  
482 better scaling that allows us to get better results. Our future work will concentrate on investigating  
483 better methods for filtering over nonuniform meshes and extending the position-dependent derivative  
484 filtering to unstructured triangular meshes.

485 **Acknowledgements**

486 The first and second authors are sponsored by the Air Force Office of Scientific Research (AFOSR),  
487 Air Force Material Command, USAF, under grant number FA8655-09-1-3017. The third author is  
488 sponsored in part by the Air Force Office of Scientific Research (AFOSR), Computational Mathematics  
489 Program (Program Manager: Dr. Fariba Fahroo), under grant number FA9550-12-1-0428. The U.S Gov-  
490 ernment is authorized to reproduce and distribute reprints for Governmental purposes notwithstanding  
491 any copyright notation thereon.

492 **References**

- 493 [1] M. Steffen, S. Curtis, R. M. Kirby, J. K. Ryan, Investigation of Smoothness-Increasing Accuracy-Conserving Filters  
494 for Improving Streamline Integration Through Discontinuous Fields, *Visualization and Computer Graphics, IEEE  
495 Transactions on* 14 (3) (2008) 680–692.
- 496 [2] J. H. Bramble, A. H. Schatz, Higher Order Local Accuracy by Averaging in the Finite Element Method, *Mathematics  
497 of Computation* 31 (137) (1977) 94–111.
- 498 [3] B. Cockburn, M. Luskin, C.-W. Shu, E. Süli, Enhanced Accuracy by Post-Processing for Finite Element Methods  
499 for Hyperbolic Equations, *Mathematics of Computation* 72 (242) (2003) 577–606.
- 500 [4] V. Thomée, High Order Local Approximations to Derivatives in the Finite Element Method, *Mathematics of Com-  
501 putation* 31 (1977) 652–660.
- 502 [5] J. K. Ryan, B. Cockburn, Local Derivative Post-Processing for the Discontinuous Galerkin Method, *Journal of  
503 Computational Physics* 228 (23) (2009) 8642–8664.
- 504 [6] S. Curtis, R. M. Kirby, J. K. Ryan, C.-W. Shu, Postprocessing for the Discontinuous Galerkin Method over Nonuni-  
505 form Meshes, *SIAM Journal on Scientific Computing* 30 (1) (2008) 272–289.
- 506 [7] J. Ryan, Local Derivative Post-processing: Challenges for a non-uniform mesh, Delft University of Technology Report  
507 10-18.
- 508 [8] J. Ryan, X. Li, R. M. Kirby, C. Vuik, One-Sided Position-Dependent Smoothness-Increasing Accuracy-Conserving  
509 (SIAC) Filtering Over Uniform and Non-Uniform Meshes, *Journal of Scientific Computing* Accepted.
- 510 [9] J. Ryan, C. W. Shu, On a One-Sided Post-Processing Technique for the Discontinuous Galerkin Methods, *Methods  
511 and Applications of analysis* 10 (2) (2003) 295–308.
- 512 [10] P. van Slingerland, J. K. Ryan, C. Vuik, Position-Dependent Smoothness-Increasing Accuracy-Conserving (SIAC)  
513 Filtering for Improving Discontinuous Galerkin Solutions, *SIAM Journal on Scientific Computing* 33 (2) (2011) 802–  
514 825.
- 515 [11] B. Cockburn, An Introduction to the Discontinuous Galerkin Method for Convection-Dominated Problems, in:  
516 A. Quarteroni (Ed.), *Advanced Numerical Approximation of Nonlinear Hyperbolic Equations*, Vol. 1697 of *Lecture  
517 Notes in Mathematics*, Springer Berlin Heidelberg, 1998, pp. 151–268.
- 518 [12] B. Cockburn, C.-W. Shu, Runge-Kutta Discontinuous Galerkin Methods for Convection-Dominated Problems, *Jour-  
519 nal of Scientific Computing* 16 (3) (2001) 173–261.
- 520 [13] C. de Boor, *A Practical Guide to Splines*, Springer-Verlag, New York, 2001.
- 521 [14] M. S. Mock, P. D. Lax, The computation of discontinuous solutions of linear hyperbolic equations, *Communications  
522 on Pure and Applied Mathematics* 31 (4) (1978) 423–430.

Table 4.1:  $L^2$ - and  $L^\infty$ -errors for the  $\alpha$ th derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions (the SRV and RLKV filters) for linear convection equation (4.1), over uniform meshes. The B-spline order is  $k + 1 + \alpha$  and the filter scaling is taken as  $H = h$ .

| Mesh            | $\partial_x^\alpha u_h$ |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) * u_h$ (SRV) |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) * u_h$ (RLKV) |       |                  |       |
|-----------------|-------------------------|-------|------------------|-------|---|-------|------------------|-------|--|-------|------------------|-------|
|                 | $L^2$ error             | order | $L^\infty$ error | order | $L^2$ error                                   | order | $L^\infty$ error | order | $L^2$ error                                    | order | $L^\infty$ error | order |
| $\alpha = 1$    |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 4.62E-01                | —     | 1.22E+00         | —     | 1.43E-02                                      | —     | 4.41E-02         | —     | 1.22E-02                                       | —     | 2.07E-02         | —     |
| 40              | 2.32E-01                | 0.99  | 6.22E-01         | 0.98  | 1.55E-03                                      | 3.20  | 2.61E-03         | 4.08  | 1.55E-03                                       | 2.97  | 4.60E-03         | 2.17  |
| 80              | 1.16E-01                | 1.00  | 3.12E-01         | 0.99  | 1.91E-04                                      | 3.02  | 2.74E-04         | 3.25  | 2.04E-04                                       | 2.92  | 1.20E-03         | 1.94  |
| 160             | 5.82E-02                | 1.00  | 1.56E-01         | 1.00  | 2.37E-05                                      | 3.01  | 3.36E-05         | 3.03  | 2.84E-05                                       | 2.84  | 3.01E-04         | 1.99  |
| 320             | 2.91E-02                | 1.00  | 7.81E-02         | 1.00  | 2.96E-06                                      | 3.01  | 4.18E-06         | 3.01  | 4.22E-06                                       | 2.75  | 7.50E-05         | 2.00  |
| $\mathcal{P}^2$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 2.19E-02                | —     | 7.97E-02         | —     | 1.40E-04                                      | —     | 9.00E-04         | —     | 4.78E-04                                       | —     | 3.09E-03         | —     |
| 40              | 5.48E-03                | 2.00  | 2.01E-02         | 1.98  | 6.69E-07                                      | 7.71  | 1.91E-06         | 8.88  | 8.14E-05                                       | 2.55  | 6.83E-04         | 2.18  |
| 80              | 1.37E-03                | 2.00  | 5.05E-03         | 2.00  | 1.69E-08                                      | 5.31  | 2.52E-08         | 6.24  | 1.44E-05                                       | 2.50  | 1.68E-04         | 2.02  |
| 160             | 3.43E-04                | 2.00  | 1.26E-03         | 2.00  | 5.13E-10                                      | 5.04  | 7.37E-10         | 5.09  | 2.54E-06                                       | 2.50  | 4.20E-05         | 2.00  |
| 320             | 8.56E-05                | 2.00  | 3.16E-04         | 2.00  | 2.14E-11                                      | 4.58  | 3.04E-11         | 4.60  | 4.50E-07                                       | 2.50  | 1.05E-05         | 2.00  |
| $\mathcal{P}^3$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 6.55E-04                | —     | 2.80E-03         | —     | 2.41E-06                                      | —     | 1.59E-05         | —     | 6.24E-06                                       | —     | 2.50E-05         | —     |
| 40              | 8.20E-05                | 3.00  | 3.53E-04         | 2.99  | 2.10E-09                                      | 10.16 | 3.89E-09         | 11.99 | 1.04E-07                                       | 5.91  | 7.61E-07         | 5.04  |
| 80              | 1.02E-05                | 3.00  | 4.42E-05         | 3.00  | 9.95E-12                                      | 7.72  | 1.63E-11         | 7.90  | 2.18E-09                                       | 5.58  | 2.99E-08         | 4.67  |
| 160             | 1.28E-06                | 3.00  | 5.53E-06         | 3.00  | 1.10E-13                                      | 6.50  | 1.62E-13         | 6.65  | 9.58E-11                                       | 4.51  | 1.78E-09         | 4.07  |
| 320             | 1.60E-07                | 3.00  | 6.92E-07         | 3.00  | 8.98E-15                                      | 3.62  | 1.27E-14         | 3.67  | 4.24E-12                                       | 4.50  | 1.11E-10         | 4.00  |
| $\alpha = 2$    |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| $\mathcal{P}^2$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 2.67E+00                | —     | 6.96E+00         | —     | 7.20E-04                                      | —     | 4.12E-03         | —     | 6.42E-02                                       | —     | 3.71E-01         | —     |
| 40              | 1.34E+00                | 1.00  | 3.50E+00         | 0.99  | 5.90E-06                                      | 6.93  | 1.73E-05         | 7.89  | 2.27E-02                                       | 1.50  | 1.74E-01         | 1.09  |
| 80              | 6.70E-01                | 1.00  | 1.75E+00         | 1.00  | 1.29E-07                                      | 5.51  | 1.83E-07         | 6.57  | 8.03E-03                                       | 1.50  | 8.67E-02         | 1.00  |
| 160             | 3.35E-01                | 1.00  | 8.78E-01         | 1.00  | 3.55E-09                                      | 5.19  | 5.02E-09         | 5.19  | 2.84E-03                                       | 1.50  | 4.33E-02         | 1.00  |
| 320             | 1.67E-01                | 1.00  | 4.39E-01         | 1.00  | 1.39E-10                                      | 4.67  | 1.97E-10         | 4.67  | 1.00E-03                                       | 1.50  | 2.17E-02         | 1.00  |
| $\mathcal{P}^3$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 1.34E-01                | —     | 4.78E-01         | —     | 6.13E-05                                      | —     | 3.87E-04         | —     | 6.48E-04                                       | —     | 4.84E-03         | —     |
| 40              | 3.36E-02                | 2.00  | 1.21E-01         | 1.99  | 2.35E-08                                      | 11.35 | 3.59E-08         | 13.39 | 1.58E-05                                       | 5.36  | 1.49E-04         | 5.03  |
| 80              | 8.40E-03                | 2.00  | 3.02E-02         | 2.00  | 1.03E-10                                      | 7.83  | 1.48E-10         | 7.93  | 1.39E-06                                       | 3.51  | 1.73E-05         | 3.10  |
| 160             | 2.10E-03                | 2.00  | 7.56E-03         | 2.00  | 8.46E-13                                      | 6.93  | 1.20E-12         | 6.95  | 1.23E-07                                       | 3.50  | 2.16E-06         | 3.00  |
| 320             | 5.25E-04                | 2.00  | 1.89E-03         | 2.00  | 5.70E-14                                      | 3.89  | 8.06E-14         | 3.89  | 1.09E-08                                       | 3.50  | 2.70E-07         | 3.00  |
| $\alpha = 3$    |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| $\mathcal{P}^3$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 1.64E+01                | —     | 4.16E+01         | —     | 3.68E-04                                      | —     | 2.26E-03         | —     | 1.74E-02                                       | —     | 1.09E-01         | —     |
| 40              | 8.19E+00                | 1.00  | 2.09E+01         | 0.99  | 1.93E-07                                      | 10.90 | 8.61E-07         | 11.36 | 3.07E-03                                       | 2.50  | 2.54E-02         | 2.10  |
| 80              | 4.10E+00                | 1.00  | 1.05E+01         | 1.00  | 7.68E-10                                      | 7.97  | 1.30E-09         | 9.38  | 5.43E-04                                       | 2.50  | 6.42E-03         | 1.99  |
| 160             | 2.05E+00                | 1.00  | 5.24E+00         | 1.00  | 5.93E-12                                      | 7.02  | 8.96E-12         | 7.18  | 9.60E-05                                       | 2.50  | 1.61E-03         | 2.00  |
| 320             | 1.02E+00                | 1.00  | 2.62E+00         | 1.00  | 8.50E-13                                      | 2.80  | 2.53E-11         | -1.50 | 1.70E-05                                       | 2.50  | 4.02E-04         | 2.00  |

Table 4.2:  $L^2$ - and  $L^\infty$ -errors for the  $\alpha$ th derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions (the SRV and RLKV filters) for linear convection equation (4.1), over uniform meshes. The B-spline order is  $k + 1$  and the filter scaling is taken as  $H = h$ .

| Mesh            | $\partial_x^\alpha u_h$ |       |                  |       | $\partial_x^\alpha u_h^*$ (SRV) |       |                  |       | $\partial_x^\alpha u_h^*$ (RLKV) |       |                  |       |
|-----------------|-------------------------|-------|------------------|-------|---------------------------------|-------|------------------|-------|----------------------------------|-------|------------------|-------|
|                 | $L^2$ error             | order | $L^\infty$ error | order | $L^2$ error                     | order | $L^\infty$ error | order | $L^2$ error                      | order | $L^\infty$ error | order |
| $\alpha = 1$    |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| 20              | 4.62E-01                | —     | 1.22E+00         | —     | 1.25E-02                        | —     | 2.52E-02         | —     | 1.45E-02                         | —     | 6.89E-02         | —     |
| 40              | 2.32E-01                | 0.99  | 6.22E-01         | 0.98  | 1.53E-03                        | 3.03  | 2.25E-03         | 3.48  | 1.91E-03                         | 2.92  | 1.28E-02         | 2.43  |
| 80              | 1.16E-01                | 1.00  | 3.12E-01         | 0.99  | 1.91E-04                        | 3.01  | 2.72E-04         | 3.05  | 2.63E-04                         | 2.86  | 2.64E-03         | 2.28  |
| 160             | 5.82E-02                | 1.00  | 1.56E-01         | 1.00  | 2.38E-05                        | 3.00  | 3.38E-05         | 3.01  | 3.84E-05                         | 2.78  | 5.90E-04         | 2.16  |
| 320             | 2.91E-02                | 1.00  | 7.81E-02         | 1.00  | 2.96E-06                        | 3.00  | 4.22E-06         | 3.00  | 5.95E-06                         | 2.69  | 1.39E-04         | 2.09  |
| $\mathcal{P}^2$ |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| 20              | 2.19E-02                | —     | 7.97E-02         | —     | 5.03E-05                        | —     | 3.23E-04         | —     | 5.66E-05                         | —     | 2.84E-04         | —     |
| 40              | 5.48E-03                | 2.00  | 2.01E-02         | 1.98  | 5.38E-07                        | 6.55  | 9.68E-07         | 8.38  | 1.05E-06                         | 5.75  | 8.34E-06         | 5.09  |
| 80              | 1.37E-03                | 2.00  | 5.05E-03         | 2.00  | 1.51E-08                        | 5.16  | 2.22E-08         | 5.44  | 2.25E-08                         | 5.55  | 2.87E-07         | 4.86  |
| 160             | 3.43E-04                | 2.00  | 1.26E-03         | 2.00  | 4.83E-10                        | 4.96  | 6.93E-10         | 5.00  | 7.49E-10                         | 4.91  | 1.39E-08         | 4.37  |
| 320             | 8.56E-05                | 2.00  | 3.16E-04         | 2.00  | 2.10E-11                        | 4.53  | 2.98E-11         | 4.54  | 3.22E-11                         | 4.54  | 8.03E-10         | 4.12  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| 20              | 6.55E-04                | —     | 2.80E-03         | —     | 9.62E-07                        | —     | 6.45E-06         | —     | 4.03E-06                         | —     | 1.64E-05         | —     |
| 40              | 8.20E-05                | 3.00  | 3.53E-04         | 2.99  | 1.34E-09                        | 9.48  | 2.51E-09         | 11.33 | 3.56E-08                         | 6.83  | 2.59E-07         | 5.98  |
| 80              | 1.02E-05                | 3.00  | 4.42E-05         | 3.00  | 6.65E-12                        | 7.66  | 1.09E-11         | 7.85  | 4.55E-10                         | 6.29  | 6.34E-09         | 5.35  |
| 160             | 1.28E-06                | 3.00  | 5.53E-06         | 3.00  | 9.66E-14                        | 6.11  | 1.41E-13         | 6.27  | 1.95E-11                         | 4.55  | 3.50E-10         | 4.18  |
| 320             | 1.60E-07                | 3.00  | 6.92E-07         | 3.00  | 8.92E-15                        | 3.44  | 1.26E-14         | 3.48  | 8.61E-13                         | 4.50  | 2.17E-11         | 4.01  |
| $\alpha = 2$    |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| $\mathcal{P}^2$ |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| 20              | 2.67E+00                | —     | 6.96E+00         | —     | 1.94E-04                        | —     | 5.41E-04         | —     | 1.14E-03                         | —     | 1.11E-02         | —     |
| 40              | 1.34E+00                | 1.00  | 3.50E+00         | 0.99  | 1.19E-05                        | 4.03  | 2.50E-05         | 4.44  | 7.49E-05                         | 3.92  | 7.18E-04         | 3.95  |
| 80              | 6.70E-01                | 1.00  | 1.75E+00         | 1.00  | 7.42E-07                        | 4.00  | 1.49E-06         | 4.07  | 6.31E-06                         | 3.57  | 8.11E-05         | 3.15  |
| 160             | 3.35E-01                | 1.00  | 8.78E-01         | 1.00  | 4.64E-08                        | 4.00  | 9.73E-08         | 3.93  | 5.45E-07                         | 3.53  | 9.89E-06         | 3.04  |
| 320             | 1.67E-01                | 1.00  | 4.39E-01         | 1.00  | 2.90E-09                        | 4.00  | 6.16E-09         | 3.98  | 4.76E-08                         | 3.52  | 1.22E-06         | 3.02  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| 20              | 1.34E-01                | —     | 4.78E-01         | —     | 5.93E-06                        | —     | 4.03E-05         | —     | 1.24E-04                         | —     | 1.02E-03         | —     |
| 40              | 3.36E-02                | 2.00  | 1.21E-01         | 1.99  | 1.04E-08                        | 9.15  | 1.91E-08         | 11.05 | 2.22E-07                         | 9.12  | 2.66E-06         | 8.58  |
| 80              | 8.40E-03                | 2.00  | 3.02E-02         | 2.00  | 5.43E-11                        | 7.58  | 1.20E-10         | 7.31  | 3.92E-10                         | 9.15  | 7.91E-09         | 8.39  |
| 160             | 2.10E-03                | 2.00  | 7.56E-03         | 2.00  | 7.45E-13                        | 6.19  | 1.70E-12         | 6.15  | 5.52E-12                         | 6.15  | 1.03E-10         | 6.27  |
| 320             | 5.25E-04                | 2.00  | 1.89E-03         | 2.00  | 5.65E-14                        | 3.72  | 9.20E-14         | 4.21  | 1.67E-13                         | 5.05  | 5.58E-12         | 4.20  |
| $\alpha = 3$    |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| $\mathcal{P}^3$ |                         |       |                  |       |                                 |       |                  |       |                                  |       |                  |       |
| 20              | 1.64E+01                | —     | 4.16E+01         | —     | 3.87E-05                        | —     | 2.55E-04         | —     | 4.23E-04                         | —     | 3.61E-03         | —     |
| 40              | 8.19E+00                | 1.00  | 2.09E+01         | 0.99  | 4.36E-07                        | 6.47  | 1.12E-06         | 7.83  | 4.26E-06                         | 6.63  | 5.85E-05         | 5.95  |
| 80              | 4.10E+00                | 1.00  | 1.05E+01         | 1.00  | 1.48E-08                        | 4.88  | 3.47E-08         | 5.01  | 8.67E-08                         | 5.62  | 1.26E-06         | 5.54  |
| 160             | 2.05E+00                | 1.00  | 5.24E+00         | 1.00  | 4.68E-10                        | 4.98  | 1.09E-09         | 5.00  | 3.73E-09                         | 4.54  | 6.67E-08         | 4.24  |
| 320             | 1.02E+00                | 1.00  | 2.62E+00         | 1.00  | 1.48E-11                        | 4.98  | 7.85E-11         | 3.79  | 1.65E-10                         | 4.50  | 4.15E-09         | 4.01  |

Table 4.3:  $L^2$ - and  $L^\infty$ -errors for the  $\alpha$ th derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions (the SRV and RLKV filters) for the Dirichlet problem (4.2), over smoothly decreasing meshes. The B-spline order is  $k + 1 + \alpha$  and the filter scaling is taken as  $H = \Delta x_j$ .

| Mesh            | $\partial_x^\alpha u_h$ |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) * u_h$ (SRV) |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) * u_h$ (RLKV) |       |                  |       |
|-----------------|-------------------------|-------|------------------|-------|---|-------|------------------|-------|--|-------|------------------|-------|
|                 | $L^2$ error             | order | $L^\infty$ error | order | $L^2$ error                                   | order | $L^\infty$ error | order | $L^2$ error                                    | order | $L^\infty$ error | order |
| $\alpha = 1$    |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 5.20E-01                | –     | 1.63E+00         | –     | 3.08E-02                                      | –     | 1.57E-01         | –     | 2.97E-02                                       | –     | 1.63E-01         | –     |
| 40              | 2.60E-01                | 1.00  | 8.31E-01         | 0.97  | 3.85E-03                                      | 3.00  | 2.33E-02         | 2.75  | 5.36E-03                                       | 2.47  | 4.38E-02         | 1.90  |
| 80              | 1.30E-01                | 1.00  | 4.14E-01         | 1.01  | 5.79E-04                                      | 2.74  | 5.28E-03         | 2.14  | 5.85E-04                                       | 3.20  | 5.22E-03         | 3.07  |
| 160             | 6.50E-02                | 1.00  | 2.08E-01         | 0.99  | 8.60E-05                                      | 2.75  | 7.98E-04         | 2.73  | 8.76E-05                                       | 2.74  | 7.47E-04         | 2.81  |
| 320             | 3.25E-02                | 1.00  | 1.04E-01         | 1.00  | 1.66E-05                                      | 2.37  | 1.08E-04         | 2.89  | 1.74E-05                                       | 2.33  | 1.37E-04         | 2.45  |
| $\mathcal{P}^2$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 3.05E-02                | –     | 1.73E-01         | –     | 4.77E-03                                      | –     | 3.21E-02         | –     | 1.74E-02                                       | –     | 1.13E-01         | –     |
| 40              | 7.63E-03                | 2.00  | 4.47E-02         | 1.95  | 4.91E-04                                      | 3.28  | 4.50E-03         | 2.83  | 3.22E-04                                       | 5.76  | 3.40E-03         | 5.05  |
| 80              | 1.91E-03                | 2.00  | 1.13E-02         | 1.98  | 1.06E-04                                      | 2.22  | 1.51E-03         | 1.57  | 3.74E-05                                       | 3.11  | 3.78E-04         | 3.17  |
| 160             | 4.78E-04                | 2.00  | 2.83E-03         | 1.99  | 1.43E-05                                      | 2.88  | 2.88E-04         | 2.40  | 6.44E-06                                       | 2.54  | 8.38E-05         | 2.17  |
| 320             | 1.19E-04                | 2.00  | 7.09E-04         | 2.00  | 1.46E-06                                      | 3.30  | 4.14E-05         | 2.80  | 1.13E-06                                       | 2.51  | 2.16E-05         | 1.95  |
| $\mathcal{P}^3$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 1.14E-03                | –     | 6.86E-03         | –     | 5.93E+00                                      | –     | 5.04E+01         | –     | 1.46E-02                                       | –     | 9.61E-02         | –     |
| 40              | 1.43E-04                | 3.00  | 8.53E-04         | 3.01  | 4.46E-05                                      | 17.02 | 7.69E-04         | 16.00 | 7.90E-06                                       | 10.85 | 7.09E-05         | 10.40 |
| 80              | 1.78E-05                | 3.00  | 1.07E-04         | 3.00  | 3.51E-06                                      | 3.67  | 5.11E-05         | 3.91  | 6.78E-08                                       | 6.86  | 8.36E-07         | 6.41  |
| 160             | 2.23E-06                | 3.00  | 1.33E-05         | 3.00  | 2.10E-07                                      | 4.06  | 4.43E-06         | 3.53  | 1.84E-09                                       | 5.21  | 2.88E-08         | 4.86  |
| 320             | 2.78E-07                | 3.00  | 1.66E-06         | 3.00  | 6.14E-09                                      | 5.10  | 1.83E-07         | 4.60  | 6.12E-11                                       | 4.91  | 1.54E-09         | 4.22  |
| $\alpha = 2$    |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| $\mathcal{P}^2$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 2.99E+00                | –     | 1.02E+01         | –     | 4.84E-01                                      | –     | 2.97E+00         | –     | 5.26E-01                                       | –     | 2.91E+00         | –     |
| 40              | 1.50E+00                | 1.00  | 5.22E+00         | 0.97  | 1.16E-01                                      | 2.07  | 1.74E+00         | 0.77  | 4.35E-02                                       | 3.60  | 3.51E-01         | 3.05  |
| 80              | 7.49E-01                | 1.00  | 2.62E+00         | 0.99  | 2.44E-02                                      | 2.24  | 3.27E-01         | 2.42  | 6.47E-03                                       | 2.75  | 5.53E-02         | 2.67  |
| 160             | 3.74E-01                | 1.00  | 1.31E+00         | 1.00  | 8.30E-03                                      | 1.56  | 1.42E-01         | 1.20  | 1.95E-03                                       | 1.73  | 1.43E-02         | 1.96  |
| 320             | 1.87E-01                | 1.00  | 6.58E-01         | 1.00  | 1.77E-03                                      | 2.23  | 4.55E-02         | 1.64  | 6.60E-04                                       | 1.56  | 8.25E-03         | 0.79  |
| $\mathcal{P}^3$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 1.82E-01                | –     | 8.31E-01         | –     | 1.46E+03                                      | –     | 1.24E+04         | –     | 7.38E+01                                       | –     | 3.08E+02         | –     |
| 40              | 4.56E-02                | 2.00  | 2.16E-01         | 1.94  | 6.52E-03                                      | 17.78 | 7.99E-02         | 17.25 | 5.15E-03                                       | 13.81 | 4.61E-02         | 12.71 |
| 80              | 1.14E-02                | 2.00  | 5.39E-02         | 2.00  | 9.28E-04                                      | 2.81  | 1.40E-02         | 2.52  | 3.61E-05                                       | 7.16  | 4.62E-04         | 6.64  |
| 160             | 2.85E-03                | 2.00  | 1.35E-02         | 2.00  | 1.17E-04                                      | 2.99  | 2.34E-03         | 2.58  | 4.14E-06                                       | 3.12  | 5.19E-05         | 3.16  |
| 320             | 7.13E-04                | 2.00  | 3.36E-03         | 2.00  | 7.19E-06                                      | 4.02  | 2.04E-04         | 3.52  | 2.51E-07                                       | 4.05  | 5.04E-06         | 3.36  |
| $\alpha = 3$    |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| $\mathcal{P}^3$ |                         |       |                  |       |   |       |                  |       |  |       |                  |       |
| 20              | 1.83E+01                | –     | 5.46E+01         | –     | 8.91E+03                                      | –     | 6.73E+04         | –     | 4.85E+05                                       | –     | 2.93E+06         | –     |
| 40              | 9.15E+00                | 1.00  | 2.78E+01         | 0.97  | 4.48E+00                                      | 10.96 | 7.35E+01         | 9.84  | 1.17E+00                                       | 18.67 | 1.65E+01         | 17.44 |
| 80              | 4.58E+00                | 1.00  | 1.39E+01         | 1.00  | 4.23E-01                                      | 3.41  | 9.44E+00         | 2.96  | 4.53E-02                                       | 4.68  | 8.75E-01         | 4.24  |
| 160             | 2.29E+00                | 1.00  | 6.96E+00         | 0.99  | 5.94E-02                                      | 2.83  | 1.12E+00         | 3.07  | 4.69E-03                                       | 3.27  | 9.29E-02         | 3.23  |
| 320             | 1.14E+00                | 1.00  | 3.48E+00         | 1.00  | 7.78E-03                                      | 2.93  | 2.08E-01         | 2.43  | 5.93E-04                                       | 2.98  | 1.09E-02         | 3.09  |

Table 4.4:  $L^2$ - and  $L^\infty$ -errors for the first derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solution  $\partial_x^\alpha u_h^*$  and  $(\partial_H^\alpha \tilde{K}_H) \star u_h$  (with the SRV filter) for linear convection equation (4.1), over Mesh 4.3. The filter scaling is taken as  $H = h^{2/5}$  near boundaries and  $H = h^{2/3}$  for interior regions (where the symmetric filter is applied).

| Mesh            | $\partial_x^\alpha u_h$ |       |                  |       | $\partial_x^\alpha u_h^*$ (SRV) |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) \star u_h$ (SRV) |       |                  |       |
|-----------------|-------------------------|-------|------------------|-------|---------------------------------|-------|------------------|-------|---|-------|------------------|-------|
|                 | $L^2$ error             | order | $L^\infty$ error | order | $L^2$ error                     | order | $L^\infty$ error | order | $L^2$ error                                       | order | $L^\infty$ error | order |
| $\alpha = 1$    |                         |       |                  |       |                                 |       |                  |       |   |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |                                 |       |                  |       |   |       |                  |       |
| 20              | 5.48E-01                | –     | 1.76E+00         | –     | 2.85E-01                        | –     | 1.49E+00         | –     | 5.91E-01  | –     | 2.54E+00         | –     |
| 40              | 2.82E-01                | 0.96  | 1.05E+00         | 0.74  | 2.63E-01                        | 0.11  | 1.57E+00         | -0.08 | 4.90E-01  | 0.27  | 2.37E+00         | 0.10  |
| 80              | 1.37E-01                | 1.05  | 4.98E-01         | 1.08  | 2.11E-01                        | 0.32  | 1.52E+00         | 0.05  | 4.17E-01  | 0.24  | 2.38E+00         | -0.00 |
| 160             | 6.72E-02                | 1.02  | 2.57E-01         | 0.96  | 1.29E-01                        | 0.71  | 1.18E+00         | 0.36  | 3.08E-01  | 0.43  | 2.30E+00         | 0.05  |
| 320             | 3.38E-02                | 0.99  | 1.30E-01         | 0.98  | 3.12E-02                        | 2.05  | 3.75E-01         | 1.65  | 9.55E-02  | 1.69  | 9.77E-01         | 1.24  |
| $\mathcal{P}^2$ |                         |       |                  |       |                                 |       |                  |       |   |       |                  |       |
| 20              | 3.56E-02                | –     | 2.01E-01         | –     | 1.15E-02                        | –     | 8.74E-02         | –     | 3.30E-02  | –     | 1.35E-01         | –     |
| 40              | 8.96E-03                | 1.99  | 5.80E-02         | 1.79  | 2.32E-03                        | 2.31  | 1.90E-02         | 2.20  | 4.21E-03  | 2.97  | 2.41E-02         | 2.49  |
| 80              | 1.96E-03                | 2.20  | 1.16E-02         | 2.32  | 2.08E-03                        | 0.16  | 1.49E-02         | 0.35  | 3.70E-03  | 0.19  | 2.34E-02         | 0.05  |
| 160             | 4.86E-04                | 2.01  | 3.88E-03         | 1.58  | 1.68E-03                        | 0.30  | 1.49E-02         | -0.00 | 3.16E-03  | 0.23  | 2.35E-02         | -0.01 |
| 320             | 1.32E-04                | 1.88  | 8.95E-04         | 2.11  | 1.36E-03                        | 0.30  | 1.50E-02         | -0.01 | 2.63E-03  | 0.27  | 2.36E-02         | -0.01 |
| $\mathcal{P}^3$ |                         |       |                  |       |                                 |       |                  |       |   |       |                  |       |
| 20              | 1.53E-03                | –     | 1.10E-02         | –     | 1.33E-02                        | –     | 7.20E-02         | –     | 4.03E-02  | –     | 2.58E-01         | –     |
| 40              | 2.10E-04                | 2.86  | 1.72E-03         | 2.68  | 7.05E-05                        | 7.56  | 3.40E-04         | 7.73  | 4.44E-05  | 9.83  | 3.07E-04         | 9.72  |
| 80              | 2.27E-05                | 3.21  | 1.80E-04         | 3.26  | 4.84E-06                        | 3.86  | 3.58E-05         | 3.25  | 6.48E-06  | 2.78  | 4.29E-05         | 2.84  |
| 160             | 2.72E-06                | 3.06  | 2.52E-05         | 2.84  | 3.30E-06                        | 0.55  | 2.89E-05         | 0.31  | 5.84E-06  | 0.15  | 4.53E-05         | -0.08 |
| 320             | 3.42E-07                | 2.99  | 3.22E-06         | 2.97  | 2.71E-06                        | 0.28  | 2.91E-05         | -0.01 | 4.97E-06  | 0.23  | 4.55E-05         | -0.01 |

Table 4.5:  $L^2$ - and  $L^\infty$ -errors for the  $\alpha$ th derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions  $\partial_x^\alpha u_h^*$  and  $(\partial_H^\alpha \tilde{K}_H) \star u_h$  (with the RLKV filter) for linear convection equation (4.1), over Mesh 4.3. The filter scaling is taken as  $H = h^{2/3}$ .

| Mesh            | $\partial_x^\alpha u_h$ |       |                  |       | $\partial_x^\alpha u_h^*$ (RLKV) |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) \star u_h$ (RLKV) |       |                  |       |
|-----------------|-------------------------|-------|------------------|-------|----------------------------------|-------|------------------|-------|--|-------|------------------|-------|
|                 | $L^2$ error             | order | $L^\infty$ error | order | $L^2$ error                      | order | $L^\infty$ error | order | $L^2$ error  | order | $L^\infty$ error | order |
| $\alpha = 1$    |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 5.48E-01                | —     | 1.76E+00         | —     | 4.19E-02                         | —     | 1.52E-01         | —     | 5.36E-02   | —     | 9.92E-02         | —     |
| 40              | 2.82E-01                | 0.96  | 1.05E+00         | 0.74  | 8.18E-03                         | 2.36  | 3.36E-02         | 2.18  | 1.14E-02   | 2.23  | 4.02E-02         | 1.30  |
| 80              | 1.37E-01                | 1.05  | 4.98E-01         | 1.08  | 1.89E-03                         | 2.11  | 6.12E-03         | 2.46  | 2.19E-03   | 2.38  | 8.22E-03         | 2.29  |
| 160             | 6.72E-02                | 1.02  | 2.57E-01         | 0.96  | 4.93E-04                         | 1.94  | 2.09E-03         | 1.55  | 3.51E-04   | 2.64  | 1.44E-03         | 2.51  |
| 320             | 3.38E-02                | 0.99  | 1.30E-01         | 0.98  | 1.46E-04                         | 1.76  | 6.15E-04         | 1.76  | 5.04E-05   | 2.80  | 2.35E-04         | 2.61  |
| $\mathcal{P}^2$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 3.56E-02                | —     | 2.01E-01         | —     | 3.13E-02                         | —     | 9.60E-02         | —     | 5.84E-02   | —     | 1.32E-01         | —     |
| 40              | 8.96E-03                | 1.99  | 5.80E-02         | 1.79  | 3.22E-04                         | 6.60  | 1.26E-03         | 6.25  | 1.04E-03   | 5.82  | 2.45E-03         | 5.75  |
| 80              | 1.96E-03                | 2.20  | 1.16E-02         | 2.32  | 7.59E-05                         | 2.08  | 4.26E-04         | 1.57  | 1.78E-04   | 2.54  | 6.73E-04         | 1.86  |
| 160             | 4.86E-04                | 2.01  | 3.88E-03         | 1.58  | 5.28E-06                         | 3.85  | 3.78E-05         | 3.49  | 1.46E-05   | 3.61  | 6.65E-05         | 3.34  |
| 320             | 1.32E-04                | 1.88  | 8.95E-04         | 2.11  | 3.20E-07                         | 4.04  | 2.60E-06         | 3.86  | 8.71E-07   | 4.07  | 4.83E-06         | 3.78  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 1.53E-03                | —     | 1.10E-02         | —     | 4.08E-03                         | —     | 1.23E-02         | —     | 5.34E-03   | —     | 1.42E-02         | —     |
| 40              | 2.10E-04                | 2.86  | 1.72E-03         | 2.68  | 8.01E-04                         | 2.35  | 2.63E-03         | 2.22  | 2.89E-03   | 0.88  | 7.96E-03         | 0.83  |
| 80              | 2.27E-05                | 3.21  | 1.80E-04         | 3.26  | 4.79E-06                         | 7.38  | 2.39E-05         | 6.78  | 3.10E-06   | 9.87  | 1.44E-05         | 9.11  |
| 160             | 2.72E-06                | 3.06  | 2.52E-05         | 2.84  | 3.62E-07                         | 3.73  | 2.03E-06         | 3.56  | 9.36E-07   | 1.73  | 4.15E-06         | 1.79  |
| 320             | 3.42E-07                | 2.99  | 3.22E-06         | 2.97  | 9.64E-09                         | 5.23  | 6.87E-08         | 4.89  | 2.71E-08   | 5.11  | 1.51E-07         | 4.78  |
| $\alpha = 2$    |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | —                       | —     | —                | —     | —                                | —     | —                | —     | 1.94E+00   | —     | 9.16E+00         | —     |
| 40              | —                       | —     | —                | —     | —                                | —     | —                | —     | 2.63E-01   | 2.89  | 1.51E+00         | 2.60  |
| 80              | —                       | —     | —                | —     | —                                | —     | —                | —     | 3.42E-02   | 2.94  | 1.99E-01         | 2.93  |
| 160             | —                       | —     | —                | —     | —                                | —     | —                | —     | 6.39E-03   | 2.42  | 2.11E-02         | 3.23  |
| 320             | —                       | —     | —                | —     | —                                | —     | —                | —     | 2.19E-03   | 1.54  | 8.55E-03         | 1.30  |
| $\mathcal{P}^2$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 3.16E+00                | —     | 9.99E+00         | —     | 3.19E-01                         | —     | 1.83E+00         | —     | 3.42E-01   | —     | 1.80E+00         | —     |
| 40              | 1.60E+00                | 0.98  | 5.79E+00         | 0.79  | 2.87E-02                         | 3.47  | 2.05E-01         | 3.16  | 1.00E-01   | 1.77  | 5.59E-01         | 1.69  |
| 80              | 7.57E-01                | 1.08  | 2.60E+00         | 1.16  | 1.11E-03                         | 4.69  | 1.21E-02         | 4.07  | 5.25E-03   | 4.25  | 3.72E-02         | 3.91  |
| 160             | 3.78E-01                | 1.00  | 1.52E+00         | 0.78  | 5.10E-04                         | 1.12  | 5.79E-03         | 1.07  | 2.07E-04   | 4.66  | 1.96E-03         | 4.24  |
| 320             | 1.96E-01                | 0.94  | 7.38E-01         | 1.04  | 2.65E-05                         | 4.26  | 2.02E-04         | 4.85  | 8.54E-06   | 4.60  | 4.75E-05         | 5.37  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 2.15E-01                | —     | 1.12E+00         | —     | 2.11E-02                         | —     | 1.39E-01         | —     | 2.21E-02   | —     | 1.21E-01         | —     |
| 40              | 5.70E-02                | 1.92  | 3.46E-01         | 1.70  | 9.02E-03                         | 1.23  | 6.45E-02         | 1.11  | 2.23E-02   | -0.01 | 1.25E-01         | -0.06 |
| 80              | 1.31E-02                | 2.12  | 7.71E-02         | 2.17  | 2.40E-04                         | 5.23  | 2.13E-03         | 4.92  | 1.15E-03   | 4.28  | 7.69E-03         | 4.03  |
| 160             | 3.17E-03                | 2.05  | 2.05E-02         | 1.91  | 3.76E-06                         | 6.00  | 4.21E-05         | 5.66  | 2.06E-05   | 5.80  | 1.71E-04         | 5.49  |
| 320             | 7.98E-04                | 1.99  | 5.27E-03         | 1.96  | 5.25E-08                         | 6.16  | 7.68E-07         | 5.78  | 2.93E-07   | 6.14  | 3.10E-06         | 5.79  |
| $\alpha = 3$    |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| $\mathcal{P}^2$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | —                       | —     | —                | —     | —                                | —     | —                | —     | 4.98E+00   | —     | 2.58E+01         | —     |
| 40              | —                       | —     | —                | —     | —                                | —     | —                | —     | 1.01E+00   | 2.31  | 5.55E+00         | 2.22  |
| 80              | —                       | —     | —                | —     | —                                | —     | —                | —     | 3.06E-02   | 5.04  | 2.73E-01         | 4.35  |
| 160             | —                       | —     | —                | —     | —                                | —     | —                | —     | 3.25E-03   | 3.24  | 2.95E-02         | 3.21  |
| 320             | —                       | —     | —                | —     | —                                | —     | —                | —     | 1.64E-03   | 0.99  | 1.66E-02         | 0.83  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 1.95E+01                | —     | 5.77E+01         | —     | 2.74E-01                         | —     | 1.78E+00         | —     | 3.40E-01   | —     | 2.21E+00         | —     |
| 40              | 9.94E+00                | 0.97  | 3.54E+01         | 0.70  | 7.63E-02                         | 1.84  | 5.36E-01         | 1.73  | 3.45E-01   | -0.02 | 2.12E+00         | 0.06  |
| 80              | 4.81E+00                | 1.05  | 1.67E+01         | 1.08  | 1.59E-03                         | 5.59  | 1.51E-02         | 5.15  | 5.12E-03   | 6.07  | 3.62E-02         | 5.87  |
| 160             | 2.37E+00                | 1.02  | 8.62E+00         | 0.96  | 3.54E-04                         | 2.17  | 4.15E-03         | 1.87  | 1.81E-04   | 4.83  | 1.73E-03         | 4.39  |
| 320             | 1.19E+00                | 0.99  | 4.37E+00         | 0.98  | 1.42E-05                         | 4.64  | 2.12E-04         | 4.29  | 6.44E-06   | 4.81  | 7.71E-05         | 4.49  |

Table 4.6:  $L^2$ - and  $L^\infty$ -errors for the  $\alpha$ th derivative of the DG approximation  $\partial_x^\alpha u_h$  together with the two filtered solutions  $\partial_x^\alpha u_h^*$  and  $(\partial_H^\alpha \tilde{K}_H) \star u_h$  (with the RLKV filter) for variable coefficient equation (4.3), over Mesh 4.4. The filter scaling is taken as  $H = h^{2/3}$ .

| Mesh            | $\partial_x^\alpha u_h$ |       |                  |       | $\partial_x^\alpha u_h^*$ (RLKV) |       |                  |       | $(\partial_H^\alpha \tilde{K}_H) \star u_h$ (RLKV) |       |                  |       |
|-----------------|-------------------------|-------|------------------|-------|----------------------------------|-------|------------------|-------|--|-------|------------------|-------|
|                 | $L^2$ error             | order | $L^\infty$ error | order | $L^2$ error                      | order | $L^\infty$ error | order | $L^2$ error  | order | $L^\infty$ error | order |
| $\alpha = 1$    |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 5.73E-01                | —     | 2.04E+00         | —     | 4.28E-02                         | —     | 9.17E-02         | —     | 4.04E-02   | —     | 8.51E-02         | —     |
| 40              | 2.76E-01                | 1.05  | 9.98E-01         | 1.03  | 1.29E-02                         | 1.73  | 6.62E-02         | 0.47  | 1.47E-02   | 1.46  | 5.53E-02         | 0.62  |
| 80              | 1.53E-01                | 0.85  | 6.35E-01         | 0.65  | 3.44E-03                         | 1.91  | 1.31E-02         | 2.34  | 2.72E-03   | 2.43  | 7.98E-03         | 2.79  |
| 160             | 7.16E-02                | 1.10  | 3.43E-01         | 0.89  | 1.01E-03                         | 1.76  | 5.63E-03         | 1.22  | 6.26E-04   | 2.12  | 1.82E-03         | 2.13  |
| 320             | 4.07E-02                | 0.82  | 2.46E-01         | 0.48  | 9.81E-04                         | 0.05  | 8.33E-03         | -0.57 | 6.37E-04   | -0.02 | 3.11E-03         | -0.77 |
| $\mathcal{P}^2$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 6.60E-02                | —     | 4.27E-01         | —     | 3.38E-02                         | —     | 1.10E-01         | —     | 6.16E-02   | —     | 1.42E-01         | —     |
| 40              | 1.27E-02                | 2.38  | 9.22E-02         | 2.21  | 3.17E-04                         | 6.73  | 1.26E-03         | 6.45  | 9.68E-04   | 5.99  | 2.46E-03         | 5.85  |
| 80              | 2.12E-03                | 2.58  | 1.27E-02         | 2.87  | 7.71E-05                         | 2.04  | 4.28E-04         | 1.55  | 1.78E-04   | 2.44  | 6.61E-04         | 1.89  |
| 160             | 6.40E-04                | 1.73  | 5.66E-03         | 1.16  | 5.33E-06                         | 3.85  | 3.71E-05         | 3.53  | 1.47E-05   | 3.60  | 6.54E-05         | 3.34  |
| 320             | 2.48E-04                | 1.37  | 2.99E-03         | 0.92  | 4.67E-07                         | 3.51  | 2.70E-06         | 3.78  | 8.72E-07   | 4.08  | 4.93E-06         | 3.73  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 2.95E-03                | —     | 2.29E-02         | —     | 4.28E-03                         | —     | 1.29E-02         | —     | 5.72E-03   | —     | 1.52E-02         | —     |
| 40              | 2.88E-04                | 3.35  | 2.84E-03         | 3.01  | 8.01E-04                         | 2.42  | 2.61E-03         | 2.31  | 2.89E-03   | 0.98  | 7.97E-03         | 0.93  |
| 80              | 3.95E-05                | 2.87  | 3.84E-04         | 2.89  | 4.82E-06                         | 7.38  | 2.36E-05         | 6.79  | 3.10E-06   | 9.87  | 1.41E-05         | 9.15  |
| 160             | 4.74E-06                | 3.06  | 6.15E-05         | 2.64  | 3.62E-07                         | 3.73  | 2.05E-06         | 3.53  | 9.36E-07   | 1.73  | 4.15E-06         | 1.76  |
| 320             | 1.28E-06                | 1.89  | 2.14E-05         | 1.52  | 9.64E-09                         | 5.23  | 6.95E-08         | 4.88  | 2.71E-08   | 5.11  | 1.51E-07         | 4.78  |
| $\alpha = 2$    |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| $\mathcal{P}^1$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | —                       | —     | —                | —     | —                                | —     | —                | —     | 2.45E+00   | —     | 1.14E+01         | —     |
| 40              | —                       | —     | —                | —     | —                                | —     | —                | —     | 4.39E-01   | 2.48  | 2.61E+00         | 2.12  |
| 80              | —                       | —     | —                | —     | —                                | —     | —                | —     | 6.57E-02   | 2.74  | 2.23E-01         | 3.55  |
| 160             | —                       | —     | —                | —     | —                                | —     | —                | —     | 3.48E-02   | 0.92  | 1.13E-01         | 0.98  |
| 320             | —                       | —     | —                | —     | —                                | —     | —                | —     | 5.99E-02   | -0.78 | 2.80E-01         | -1.31 |
| $\mathcal{P}^2$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 3.89E+00                | —     | 1.40E+01         | —     | 3.34E-01                         | —     | 2.36E+00         | —     | 3.39E-01   | —     | 2.26E+00         | —     |
| 40              | 1.78E+00                | 1.13  | 6.49E+00         | 1.10  | 2.93E-02                         | 3.51  | 2.23E-01         | 3.40  | 1.03E-01   | 1.72  | 5.84E-01         | 1.95  |
| 80              | 7.66E-01                | 1.22  | 2.54E+00         | 1.35  | 1.11E-03                         | 4.72  | 9.19E-03         | 4.60  | 5.31E-03   | 4.28  | 3.73E-02         | 3.97  |
| 160             | 4.10E-01                | 0.90  | 1.86E+00         | 0.45  | 2.28E-04                         | 2.28  | 1.26E-03         | 2.87  | 1.86E-04   | 4.84  | 1.62E-03         | 4.52  |
| 320             | 2.28E-01                | 0.85  | 1.36E+00         | 0.45  | 2.00E-04                         | 0.19  | 1.38E-03         | -0.14 | 1.39E-05   | 3.74  | 8.73E-05         | 4.22  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 2.89E-01                | —     | 1.67E+00         | —     | 2.16E-02                         | —     | 1.63E-01         | —     | 1.84E-02   | —     | 1.13E-01         | —     |
| 40              | 6.24E-02                | 2.21  | 4.20E-01         | 1.99  | 9.03E-03                         | 1.26  | 6.49E-02         | 1.33  | 2.22E-02   | -0.28 | 1.25E-01         | -0.15 |
| 80              | 1.80E-02                | 1.79  | 1.27E-01         | 1.72  | 2.35E-04                         | 5.27  | 2.09E-03         | 4.96  | 1.15E-03   | 4.28  | 7.60E-03         | 4.04  |
| 160             | 4.12E-03                | 2.13  | 3.67E-02         | 1.79  | 3.66E-06                         | 6.00  | 4.28E-05         | 5.61  | 2.06E-05   | 5.80  | 1.73E-04         | 5.46  |
| 320             | 1.51E-03                | 1.45  | 1.79E-02         | 1.03  | 1.06E-07                         | 5.10  | 7.61E-07         | 5.81  | 2.93E-07   | 6.14  | 3.11E-06         | 5.80  |
| $\alpha = 3$    |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| $\mathcal{P}^2$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | —                       | —     | —                | —     | —                                | —     | —                | —     | 6.75E+00   | —     | 4.36E+01         | —     |
| 40              | —                       | —     | —                | —     | —                                | —     | —                | —     | 1.18E+00   | 2.51  | 7.23E+00         | 2.59  |
| 80              | —                       | —     | —                | —     | —                                | —     | —                | —     | 2.36E-02   | 5.65  | 2.19E-01         | 5.04  |
| 160             | —                       | —     | —                | —     | —                                | —     | —                | —     | 7.55E-03   | 1.64  | 7.38E-02         | 1.57  |
| 320             | —                       | —     | —                | —     | —                                | —     | —                | —     | 1.28E-03   | 2.57  | 7.79E-03         | 3.24  |
| $\mathcal{P}^3$ |                         |       |                  |       |                                  |       |                  |       |  |       |                  |       |
| 20              | 2.04E+01                | —     | 6.86E+01         | —     | 1.68E+00                         | —     | 1.10E+01         | —     | 2.37E+00   | —     | 1.56E+01         | —     |
| 40              | 9.76E+00                | 1.06  | 3.31E+01         | 1.05  | 9.36E-02                         | 4.17  | 6.06E-01         | 4.18  | 3.52E-01   | 2.75  | 2.16E+00         | 2.85  |
| 80              | 5.39E+00                | 0.86  | 2.14E+01         | 0.63  | 4.87E-04                         | 7.59  | 3.77E-03         | 7.33  | 5.15E-03   | 6.10  | 3.73E-02         | 5.86  |
| 160             | 2.52E+00                | 1.10  | 1.15E+01         | 0.89  | 1.55E-04                         | 1.65  | 1.84E-03         | 1.04  | 1.76E-04   | 4.87  | 1.73E-03         | 4.43  |
| 320             | 1.39E+00                | 0.86  | 7.30E+00         | 0.66  | 6.97E-05                         | 1.16  | 5.24E-04         | 1.81  | 6.60E-06   | 4.74  | 7.91E-05         | 4.45  |

Table 5.1:  $L^2$  – and  $L^\infty$  –errors for the cross-derivative DG approximation  $\partial_{xy}^2 u_h$  together with the filtered solutions for the two-dimensional linear convection equation (5.1) over Mesh 4.3 (2D).

| Mesh            | $\partial_{xy}^2 u_h$ |       |                  |       | $\partial_{xy}^2 u_h^* \text{ (RLKV)}$ |       |                  |       | $(\partial_{H_x} \partial_{H_y} \tilde{K}_H) \star u_h \text{ (RLKV)}$ |       |                  |       |
|-----------------|-----------------------|-------|------------------|-------|--|-------|------------------|-------|--|-------|------------------|-------|
|                 | $L^2$ error           | order | $L^\infty$ error | order | $L^2$ error                            | order | $L^\infty$ error | order | $L^2$ error  | order | $L^\infty$ error | order |
| $\mathcal{P}^1$ |                       |       |                  |       |  |       |                  |       |  |       |                  |       |
| 20 × 20         | 5.47E+00              | –     | 2.32E+01         | –     | –                                      | –     | –                | –     | 1.32E+00   | –     | 1.25E+01         | –     |
| 40 × 40         | 2.71E+00              | 1.01  | 1.33E+01         | 0.81  | –                                      | –     | –                | –     | 1.97E-01   | 2.75  | 1.80E+00         | 2.79  |
| 80 × 80         | 1.33E+00              | 1.03  | 6.39E+00         | 1.06  | –                                      | –     | –                | –     | 2.81E-02   | 2.81  | 2.56E-01         | 2.81  |
| 160 × 160       | 6.62E-01              | 1.00  | 3.38E+00         | 0.92  | –                                      | –     | –                | –     | 4.08E-03   | 2.78  | 3.39E-02         | 2.92  |
| $\mathcal{P}^2$ |                       |       |                  |       |  |       |                  |       |  |       |                  |       |
| 20 × 20         | 3.48E-01              | –     | 2.49E+00         | –     | 4.68E-01                               | –     | 3.44E+00         | –     | 5.66E-01   | –     | 3.59E+00         | –     |
| 40 × 40         | 8.16E-02              | 2.09  | 7.13E-01         | 1.80  | 2.65E-02                               | 4.14  | 3.63E-01         | 3.24  | 5.38E-02   | 3.40  | 6.81E-01         | 2.40  |
| 80 × 80         | 1.93E-02              | 2.08  | 1.81E-01         | 1.98  | 1.38E-03                               | 4.26  | 1.96E-02         | 4.22  | 2.83E-03   | 4.25  | 4.03E-02         | 4.08  |
| 160 × 160       | 4.79E-03              | 2.01  | 4.53E-02         | 2.00  | 6.86E-05                               | 4.33  | 8.74E-04         | 4.48  | 1.44E-04   | 4.30  | 1.84E-03         | 4.45  |
| $\mathcal{P}^3$ |                       |       |                  |       |  |       |                  |       |  |       |                  |       |
| 20 × 20         | 1.54E-02              | –     | 1.47E-01         | –     | 4.11E-02                               | –     | 2.79E-01         | –     | 4.06E-02   | –     | 2.63E-01         | –     |
| 40 × 40         | 1.75E-03              | 3.13  | 2.29E-02         | 2.68  | 1.14E-02                               | 1.85  | 1.27E-01         | 1.13  | 2.45E-02   | 0.73  | 2.04E-01         | 0.37  |
| 80 × 80         | 2.00E-04              | 3.13  | 2.51E-03         | 3.19  | 2.42E-04                               | 5.56  | 4.26E-03         | 4.90  | 5.30E-04   | 5.53  | 8.51E-03         | 4.58  |
| 160 × 160       | 2.47E-05              | 3.02  | 3.58E-04         | 2.81  | 4.91E-06                               | 5.62  | 8.59E-05         | 5.63  | 1.08E-05   | 5.62  | 1.81E-04         | 5.56  |

Table 5.2:  $L^2$  – and  $L^\infty$  –errors for the cross-derivative DG approximation  $\partial_{xy}^2 u_h$  together with the filtered solutions for the two-dimensional linear advection equation (5.1) over Mesh 4.4 (2D).

| Mesh            | $\partial_{xy}^2 u_h$ |       |                  |       | $\partial_{xy}^2 u_h^* \text{ (RLKV)}$ |       |                  |       | $(\partial_{H_x} \partial_{H_y} \tilde{K}_H) \star u_h \text{ (RLKV)}$ |       |                  |       |
|-----------------|-----------------------|-------|------------------|-------|--|-------|------------------|-------|--|-------|------------------|-------|
|                 | $L^2$ error           | order | $L^\infty$ error | order | $L^2$ error                            | order | $L^\infty$ error | order | $L^2$ error  | order | $L^\infty$ error | order |
| $\mathcal{P}^1$ |                       |       |                  |       |  |       |                  |       |  |       |                  |       |
| 20 × 20         | 6.03E+00              | –     | 2.94E+01         | –     | –                                      | –     | –                | –     | 1.53E+00   | –     | 1.27E+01         | –     |
| 40 × 40         | 3.20E+00              | 0.91  | 1.95E+01         | 0.59  | –                                      | –     | –                | –     | 2.72E-01   | 2.50  | 2.07E+00         | 2.62  |
| 80 × 80         | 1.61E+00              | 0.99  | 1.09E+01         | 0.84  | –                                      | –     | –                | –     | 5.44E-02   | 2.32  | 4.01E-01         | 2.37  |
| 160 × 160       | 7.39E-01              | 1.12  | 5.18E+00         | 1.07  | –                                      | –     | –                | –     | 8.35E-03   | 2.70  | 1.37E-01         | 1.55  |
| $\mathcal{P}^2$ |                       |       |                  |       |  |       |                  |       |  |       |                  |       |
| 20 × 20         | 5.60E-01              | –     | 7.00E+00         | –     | 4.73E-01                               | –     | 3.48E+00         | –     | 5.68E-01   | –     | 3.59E+00         | –     |
| 40 × 40         | 1.68E-01              | 1.73  | 2.65E+00         | 1.40  | 2.67E-02                               | 4.15  | 3.67E-01         | 3.24  | 5.34E-02   | 3.41  | 6.88E-01         | 2.38  |
| 80 × 80         | 3.85E-02              | 2.13  | 5.30E-01         | 2.32  | 1.36E-03                               | 4.29  | 1.94E-02         | 4.24  | 2.98E-03   | 4.16  | 4.12E-02         | 4.06  |
| 160 × 160       | 7.27E-03              | 2.41  | 1.03E-01         | 2.37  | 7.90E-05                               | 4.11  | 1.05E-03         | 4.21  | 1.54E-04   | 4.27  | 1.89E-03         | 4.44  |
| $\mathcal{P}^3$ |                       |       |                  |       |  |       |                  |       |  |       |                  |       |
| 20 × 20         | 4.02E-02              | –     | 3.66E-01         | –     | 4.12E-02                               | –     | 2.79E-01         | –     | 4.05E-02   | –     | 2.64E-01         | –     |
| 40 × 40         | 7.60E-03              | 2.40  | 1.03E-01         | 1.83  | 1.14E-02                               | 1.86  | 1.29E-01         | 1.12  | 2.45E-02   | 0.72  | 2.06E-01         | 0.36  |
| 80 × 80         | 7.71E-04              | 3.30  | 1.68E-02         | 2.61  | 2.42E-04                               | 5.55  | 4.21E-03         | 4.93  | 5.30E-04   | 5.53  | 8.40E-03         | 4.62  |
| 160 × 160       | 5.76E-05              | 3.74  | 1.31E-03         | 3.69  | 4.91E-06                               | 5.62  | 8.65E-05         | 5.60  | 1.08E-05   | 5.62  | 1.82E-04         | 5.51  |